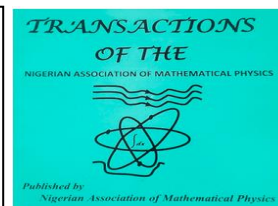


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THE DYNAMIC BUCKLING LOAD FORMULA OF A CUBIC MODEL STRUCTURE STRUCK BY SLOWLY VARYING FREQUENCY

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ABSTRACT

This investigation is centred on an analytical determination of the dynamic buckling loads formula of some viscously damped elastic structures pressurized by a periodic load with slowly varying circular frequencies. The formulation has two small but mathematically independent parameters which allow the use of asymptotic expansions of the variables. In addition, a two-timing regular perturbation procedure is used to analyze the relevant equations which contain some degrees of nonlinearities in their formulation. The dynamic buckling load, λ_D lies between 0 and 1, $0 < \lambda_D \ll 1$.

1.1 BACKGROUND OF STUDY

In this study, we are aiming at finding the dynamic buckling loads of some imperfect elastic structures having light viscous damping but trapped by a periodic load with slowly varying circular frequency. The analysis is based on already existing theory derived by [1] and [2]. The two structures studied by [3] are the simple cubic elastic model structure and an imperfect elastic spherical cap whose normal displacement is regarded as the summation of the modes, that is, pre-buckling, an axis symmetric and non-axis symmetric modes, all having time dependent amplitudes. The theory is here developed through the simple cubic elastic model structure followed by a practical application on an elastic spherical cap, where all deformations (failures) are controlled within elastic range. The problems derived are non-linear which need to be solved but there is no simple analytical method to handle the solutions. We choose perturbation method to handle the problem because of the presence of two small mathematically independent parameters through which a two-timing perturbation scheme is formed. In the same vein, the problem now becomes a two-small parameter non-linear problem, which the solution here can be approached analytically using regular perturbation and asymptotic methods.

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In most countries of the world we often hear of collapse of buildings, bridges and other material structures. These are forms of material failures which are dangerous in nature and should be prevented by all cost. Great investigations and efforts have been done by Engineers and Applied Mathematicians to determine the maximum loads that structures can carry before buckling occurs but still, buckling of elastic structures still comes to play from time to time. The dynamic buckling analysis of imperfect spherical shell with light viscous damping trapped by a periodic load with slowly varying frequency, is a real life problem, yet, it does not seem, to our knowledge, that a lot of analytical investigations have been done on the subject matter. Most of the earlier works done on this area, used numerical methods (Finite Element methods) for the analysis of buckling. In this study, we are carrying out investigations using purely analytical methods to investigate the dynamic buckling and stability of two viscously damped elastic structures, namely, a simple cubic model and an imperfect elastic spherical shell pressurized by a periodic load that has a slowly varying frequency. In addition, we investigate the effect of light viscous damping on the dynamic stability of the structures.

The concept of dynamic buckling is presently an interesting area of research which many researchers have gone into based on the reality that it is closely related to some other fields of human endeavor. Structural elastic materials have the tendencies of undergoing deformations and other instabilities when loaded either statically or dynamically. One of the major concerns of structural Engineers and Applied Mathematicians is to know the load carrying capacity of a given elastic material before buckling. Many researchers have worked on dynamic stability of structures by subjecting these materials to various loading conditions. We recall that [1] studied the step loading, impulse loading, rectangular loading and triangular loading while [2] analyzed the impact of periodic loading on elastic structures. Based on researches conducted by many investigators some of which are [1],[2] and others, it has become clear that initial imperfections, the loading history (i.e. the nature of the loading), the time duration and the elastic characteristics of materials affect the dynamic buckling loads of structures. To our knowledge, periodic loading with slowly varying circular frequency is not commonly discussed in the area of buckling. It is however quite pertinent to mention that the concept of periodic forcing with slowly varying frequency in the time variables was discussed by [4]. In that study, the frequency was assumed to have a slow cubic variation with time and was discussed in the context of a weakly damped and weakly non-linear excitation involving Duffing's equation.

Currently, most studies on dynamic buckling appear to centre on beams, plates, columns, spherical shells and cylindrical shells with extensive literatures and the techniques adopted are mostly numerical approach. In view of this, mention must be made of [5], who studied the dynamic buckling of thin – walled viscoplastic columns while [6], similarly studied some aspects of dynamic buckling of plates under in-plane pulse compression. In the same way, [7], studied some important parameters in dynamic buckling analysis of plated structures subjected to impulse loading, [8], investigated Asymptotic investigation of the buckling of a cubic-quintic nonlinear elastic model structure stressed by static load and a dynamic step load, [9] studied the imperfect Bifurcation with a slowly – vary control parameter while [2], studied the buckling of impulsively loaded prismatic cores. Worthy of mentioning are [10], who investigated the stability of transverse vibration of rod under longitudinal step wise loading, [11] who investigated advances in shell buckling theory and experiments, [2], studied dynamic buckling estimates and [12] who investigated the influence of uncertainties on the dynamic buckling loads of structures liable to Asymmetric post buckling behavior. The study of buckling behavior of beams and columns was studied by [13], a study on buckling – waves was carried out by [14] while [15] dealt on the dynamic buckling of a model structure with quadratic non-linearity struck by a step load superposed on Quasi- static load. The investigation into the dynamic effects of lateral buckling of high temperature/High pressure offshore pipelines was carried out by [16], while [17] investigated the dynamic buckling of shallow pin-ended arches under a sudden central concentrated load. In the same manner, [18] carried out investigation on elastic buckling of steel columns under axial compression, [19] studied elastic buckling of columns with end restraint effects, [20] conducted an investigation on analytic approach for exactly determining critical loads of buckling of non-uniform columns while [21], investigated the buckling of variables section columns under axial loading.

The following investigations are equally of relevance in this work : [22] who studied perturbation technique in the buckling of some elastic materials struck by a periodic load with slowly varying frequency in which this work is an obvious extension by assuming light viscous damping, [23] investigated the dynamics of rods under axial impact, [24] embarked on numerical methods for determining strongest cantilever beam with constant volume, [25] studied nonlinear stochastic dynamical post buckling analysis of uncertain cylindrical shells, [26] investigated dynamic buckling of composite cylindrical shell subjected to axial impulse while [27] conducted a research on numerical and experimental stability of buckling of advanced fibre composite cylinders under axial compression. In the same vein,

[28] investigated dynamic buckling of an inclined structure, [29] studied the dynamic buckling of thin thermovisplastic rectangular plate, [30] researched on the buckling of a clamped viscously damped column trapped by a step load, [39] researched on the buckling load of elastic quadratic non-linear structures by an axial impulse while [31] worked on analysis of tilt- buckling of Euler columns with varying flexural stiffness using homotopy perturbation method. Furthermore, [32] made remarkable contributions to the field on vibration analysis of cracked frame structures, [33] conducted research on the comparison of critical buckling load in regression, fuzzy logic and ANN based estimations while [34] studied buckling analysis of a beam-column using multilayer perception neural network technique. We note that [35] investigated the determination of buckling loads and mode shapes of heavy vertical column under its own weights using variational iteration method , [36] carried out a research on buckling of axially loaded castellated steel columns while [37] made a contribution on a simple method to determine the critical loads for axially in- homogenous beams with elastic restraints, [38] carried out an investigation on the buckling of Euler columns with a continuous elastic restraint via homotopy analysis method, [39] gave the solution for the problem of a new FEM procedure for transverse and longitudinal vibration analysis of thin rectangular plates subjected to a variable velocity moving load along an arbitrary trajectory and [40] investigated the asymptotic analysis of an improved quadratic model structure subjected to static loading. In the same way, [41] investigated the shape optimization of damaged columns subjected to conservative and non-conservative forces, [42] made investigation on maximum load factor corresponding to a slightly asymmetric bifurcation point, [43] studied an analytical formulation for local buckling and postbuckling analysis of stiffened laminated panels, [44] investigated the optimal design of clamped columns for stability under combined axial compression and torsion while [8] studied the asymptotic analysis of the static buckling of infinitely long and harmonically imperfect column lying on quadratic- cubic elastic foundations.

2.0 METHODOLOGY

The methodology applied in this work is anchored on regular perturbation and asymptotic analysis. The type of problem solved automatically demands the use of these methods. The two problems confronted in this work are non-linear and so, we cannot determine their exact analytical solutions in a closed form. The formulations in both cases have two small mathematically independent parameters in which asymptotic series expansions are used in this work. To get a uniformly valid asymptotic solution in each case, we shall apply two-timing regular perturbation techniques in the two problems. Expansions are asymptotic and are valid in the limit as the two small parameters become very small compared to unity. Usually, in most multi-timing perturbation problems, the use of two timing procedure converts the ordinary differential equations in which the problems were originally posed, to partial differential equations.

In each of these two problems, our initial intention is to get the displacement, and later, the maximum displacement, η_a . The condition for buckling (i.e. at maximum displacement), as in [2] is

$$\frac{d\lambda}{d\eta_a} = 0 \tag{2.1}$$

This is to be evaluated to get the dynamic buckling, λ_D .

The dynamic buckling load λ_D is the largest load parameter for the problem to have a bounded solution.

2.1 FORMULATION OF THE SIMPLE MODEL PROBLEM

DETERMINATION OF THE DYNAMIC BUCKLING LOAD IN THE CASE OF CUBIC MODEL STRUCTURE

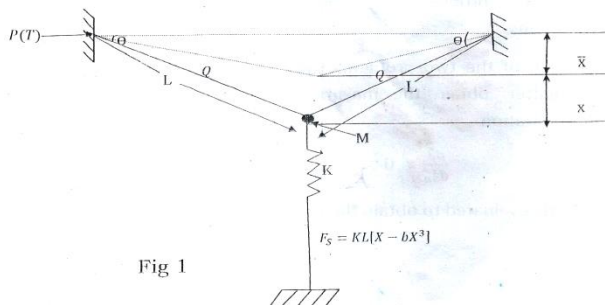


Fig 1

SIMPLE CUBIC MODEL STRUCTURE

We consider a simple model in the form of two bars of equal length L which fixed at both ends to the rigid wall as shown in the figure 1 above. The bars are subjected to a horizontal load $P(T)$ applied shortly after time $T = 0$. The bar must be rigid to avoid deformation when load is applied. A mass M is suspended at the meeting point of the two arms of the bars whose movement is regulated by a non-linear (cubic) spring that gives a restoring force F_s per unit length of $KL(X - bX^3)$, $b > 0$ where K is a spring constant, where X is the additional displacement from the point of equilibrium. Let \bar{X} be the imperfection parameter when the two arms of the bars are joined in the horizontal direction. Let Q be the tension (force) on the each arm of the bars and θ be the angle between the horizontal direction and each arm of the bars.

We assume that θ must be small relative to unity. Therefore we make the following approximations

$$\sin \theta = \frac{\bar{X} + X}{L}, \quad \sin \theta \cong \theta$$

$$\therefore \theta = \frac{\bar{X} + X}{L} \quad (2.2)$$

It is to be noted that $P(T)$ on the horizontal axis relates with the tension Q on each arm of the bars. For equilibrium of the forces on the axial direction where $P(T)$ acts, we obtain

$$\cos \theta = \frac{P(T)}{Q}, \quad P(T) = Q \cos \theta \quad (2.3a,b)$$

For equilibrium of forces in the vertical direction, where mass M acts, we have

$$F_y = 2Q \sin \theta \quad (2.4)$$

The restoring force of the spring is,

$$F_s = KL \left(\frac{X}{L} - b \left(\frac{X}{L} \right)^3 \right) \quad (2.5)$$

The net vertical force is,

$$F = F_y - F_s \quad (2.6)$$

According to Newton's law of motion

$$F = Ma = \frac{M}{L} \frac{d^2 X}{dT^2} \quad (2.7a)$$

where a is the acceleration, hence, (3.7a) becomes,

$$\frac{M}{L} \frac{d^2 X}{dT^2} = F \quad (2.7b)$$

Substituting (2.4), (2.5) in (2.6), gives,

$$F = 2Q \sin \theta - KL \left(\frac{X}{L} - b \left(\frac{X}{L} \right)^3 \right) \quad (2.8)$$

Hence, substituting (2.8) in (2.7b), gives,

$$\frac{M}{L} \frac{d^2 X}{dT^2} = 2Q \sin \theta - KL \left(\frac{X}{L} - b \left(\frac{X}{L} \right)^3 \right) \quad (2.9)$$

Then, (2.3b), becomes,

$$P(T) = Q \quad (2.10)$$

Substituting (2.2) and (2.10) in (2.9), gives

$$\begin{aligned} \frac{M}{L} \frac{d^2 X}{dT^2} &= 2P(T) \left(\frac{\bar{X} + X}{L} \right) - KL \left(\frac{X}{L} - b \left(\frac{X}{L} \right)^3 \right) = 2P(T) \frac{\bar{X}}{L} + 2P(T) \frac{X}{L} - KL \frac{X}{L} + bKL \left(\frac{X}{L} \right)^3 \\ &= 2P(T) \frac{\bar{X}}{L} + KL \frac{X}{L} \left(\frac{2P(T)}{KL^2} - 1 \right) + bKL \left(\frac{X}{L} \right)^3 \end{aligned} \quad (2.11)$$

From (2.11), we make $2P(T) \frac{\bar{X}}{L}$ the subject and get

$$\frac{M}{L} \frac{d^2 X}{dT^2} + KL \left(1 - \frac{2P(T)}{KL^2} \right) \frac{X}{L} - bKL \left(\frac{X}{L} \right)^3 = \frac{2P(T)\bar{X}}{L} \quad (2.12)$$

Now it is pertinent to introduce the following non-linear dimensional equations,

$$\eta = \frac{X}{L}; \quad \epsilon = \frac{\bar{X}}{L}; \quad t = T \sqrt{\frac{KL}{M}}, \quad 0 < \epsilon \ll 1 \quad (2.13)$$

Let,

$$2P(T) = \frac{2P(T)P(0)}{P(0)} = 2f(t)P(0) \quad (2.14)$$

where,

$$f(t) = \frac{P(T)}{P(0)}; \lambda = \frac{2P(0)}{KL^2}; P(0) \neq 0 \quad (2.15)$$

Substituting (2.13), (2.14) and (2.15) in (2.12), the results gives

$$M \left(\frac{KL^2}{M} \right) \frac{d^2 \eta}{dt^2} + KL \left(1 - \frac{2f(t)P(0)}{KL^2} \right) \eta - KLb(\eta)^3 = 2\epsilon f(t)P(0)$$

This implies that,

$$KL^2 \frac{d^2 \eta}{dt^2} + KL^2 \left(1 - \frac{2f(t)P(0)}{KL^2} \right) \eta - KbL^2\eta^3 = 2\epsilon f(t)P(0) \quad (2.16)$$

After simplifying (2.16) using (2.13)-(2.15), (2.16) becomes,

$$\frac{d^2 \eta}{dt^2} + (1 - \lambda f(t))\eta - b\eta^3 = \lambda \epsilon f(t); t > 0 \quad (2.17a)$$

$$\eta(0) = \frac{d\eta(0)}{dt} \quad (2.17b)$$

Equation(2.17a) is the required equation of motion for all types of loading $\lambda f(t)$. It was first derived by [2]

For our work, $\lambda f(t)$ is periodic load with slowly varying frequency with amplitude λ . We let,

$$f(t) = \text{Cos}(\omega(\delta t)); 0 < t < \infty; 0 < \delta \ll 1 \quad (2.18)$$

where $\omega(\delta t)$ is a continuous slowly varying time dependent frequency function

with right hand derivatives of all orders at $t = 0$ and is such that

$$\omega(0) = 0; |\omega(\delta t)| \ll 1; 0 < \delta \ll 1.$$

Then, the relevant equation of motion (2.17a), which is here adjusted to include a light viscous damping now becomes

$$\frac{d^2 \eta}{dt^2} + 2\delta \frac{d\eta}{dt} + (1 - \lambda \cos(\omega(\delta t)))\eta - b\eta^3 = \lambda \epsilon \cos(\omega(\delta t)) \quad (2.19a)$$

where b is the imperfection - sensitivity parameter and $2\delta \frac{d\eta}{dt}$ is the damping term with coefficient 2δ . The damping is said to be light because of the coefficient 2δ is such that $0 < \delta \ll 1$.

We now let,

$$\tau = \delta t \quad (2.19b)$$

$$\therefore \omega = \omega(\delta t) = \omega(\tau) \quad (2.20a)$$

The general equation (2.19a) forms a second order non-linear, non-homogenous differential equation with slowly varying time-dependent and periodic co-efficient where τ is a slow time scale and δ is small compared to unity .

Here, λ is load parameter, for $0 < \lambda < 1$, η is the deflection (displacement)

Now, we let,

$$\frac{d\tilde{t}}{dt} = [1 - \lambda \cos(\omega(\delta t))]^{1/2} = [1 - \lambda \cos(\omega(\tau))]^{1/2} \quad (2.20b)$$

$$\hat{t} = \tilde{t} + \frac{1}{\delta} \left\{ \sum_{i=1}^n \mu_i(\tau) \epsilon^i \right\} = \tilde{t} + \frac{1}{\delta} [\mu_1(\tau)\epsilon + \mu_2(\tau)\epsilon^2 + \dots] \quad (2.20c)$$

where,

$$\mu_i(0) = 0; i = 1, 2, 3, \dots$$

Therefore, we have,

$$\frac{d\eta}{dt} = \frac{\partial \eta}{\partial \hat{t}} \frac{\partial \hat{t}}{\partial \tilde{t}} \frac{\partial \tilde{t}}{\partial t} + \frac{\partial \eta}{\partial \hat{t}} \frac{\partial \hat{t}}{\partial \tau} \frac{d\tau}{dt} + \frac{\partial \eta}{\partial \tau} \frac{d\tau}{dt} \quad (2.21a)$$

We note that,

$$\frac{\partial \eta}{\partial \hat{t}} = \eta_{,\hat{t}}; \frac{\partial \hat{t}}{\partial \tilde{t}} = 1; \frac{\partial \eta}{\partial \tau} = \eta_{,\tau}; \frac{d\tau}{dt} = \delta$$

$$\frac{\partial \hat{t}}{\partial \tau} = \frac{1}{\delta} (\mu'_1 \epsilon + \mu'_2 \epsilon^2 + \mu'_3 \epsilon^3 + \dots) \quad (2.21b)$$

Here a subscript following a comma indicates partial differentiation and

$$\frac{d(\dots)}{d\tau} = (\dots)'$$

Substituting (2.21b) in (2.21a), we obtain,

$$\begin{aligned} \frac{d\eta}{dt} &= (1 - \lambda \cos(\omega(\tau)))^{1/2} \eta_{,\hat{t}} + \frac{1}{\delta} (\mu'_1 \epsilon + \mu'_2 \epsilon^2 + \mu'_3 \epsilon^3 + \dots) \delta \eta_{,\hat{t}} + \delta \eta_{,\tau} \\ &= (1 - \lambda \cos(\omega(\tau)))^{1/2} \eta_{,\hat{t}} + (\mu'_1 \epsilon + \mu'_2 \epsilon^2 + \mu'_3 \epsilon^3 + \dots) \eta_{,\hat{t}} + \delta \eta_{,\tau} \end{aligned} \quad (2.21c)$$

Hence forth, we shall write $\cos(\omega(\tau))$ simply as $\cos(\omega)$

Then, it follows that,

$$\begin{aligned} \frac{d^2\eta}{dt^2} &= (1 - \lambda \cos(\omega)) \eta_{,\hat{t}\hat{t}} + 2(1 - \lambda \cos(\omega))^{1/2} (\mu'_1 \epsilon + \mu'_2 \epsilon^2 + \dots) \eta_{,\hat{t}\hat{t}} \\ &+ (\mu'_1 \epsilon + \mu'_2 \epsilon^2 + \dots)^2 \eta_{,\hat{t}\hat{t}} + 2\delta(1 - \lambda \cos(\omega))^{1/2} \eta_{,\hat{t}\tau} + 2\delta(\mu'_1 \epsilon + \mu'_2 \epsilon^2 + \mu'_3 \epsilon^3 + \dots) \eta_{,\hat{t}\tau} \\ &+ \frac{\delta \lambda \omega' \sin(\omega)}{2(1 - \lambda \cos(\omega))^{1/2}} \eta_{,\hat{t}} + \delta^2 \eta_{,\tau\tau} + (\mu''_1 \epsilon + \mu''_2 \epsilon^2 + \mu''_3 \epsilon^3 + \dots) \eta_{,\hat{t}} \end{aligned} \quad (2.22a)$$

It is to be recalled that the relevant equation is,

$$\frac{d^2\eta}{dt^2} + 2\delta \frac{d\eta}{dt} + (1 - \lambda \cos(\omega)) \eta - b\eta^3 = \lambda \epsilon \cos(\omega) \quad (2.22b)$$

Substituting (2.21c) and (2.22a) in (2.22b), leads to,

$$\begin{aligned} & \left[(1 - \lambda \cos(\omega)) \eta_{,\hat{t}\hat{t}} + 2(1 - \lambda \cos(\omega))^{1/2} (\mu'_1 \epsilon + \mu'_2 \epsilon^2 + \mu'_3 \epsilon^3 + \dots) \eta_{,\hat{t}\hat{t}} \right. \\ & + (\mu'_1 \epsilon + \mu'_2 \epsilon^2 + \mu'_3 \epsilon^3 + \dots)^2 \eta_{,\hat{t}\hat{t}} + 2\delta(1 - \lambda \cos(\omega))^{1/2} \eta_{,\hat{t}\tau} + 2\delta(\mu'_1 \epsilon + \mu'_2 \epsilon^2 \\ & \quad \left. + \mu'_3 \epsilon^3 + \dots) \eta_{,\hat{t}\tau} + \frac{\lambda \delta \omega' \sin(\omega)}{2(1 - \lambda \cos(\omega))^{1/2}} \eta_{,\hat{t}} + \delta^2 \eta_{,\tau\tau} + (\mu''_1 \epsilon + \mu''_2 \epsilon^2 + \mu''_3 \epsilon^3 + \dots) \eta_{,\hat{t}} \right] \\ & + 2\delta \left[(1 - \lambda \cos(\omega))^{1/2} \eta_{,\hat{t}} + (\mu'_1 \epsilon + \mu'_2 \epsilon^2 + \mu'_3 \epsilon^3 + \dots) \eta_{,\hat{t}} + \delta \eta_{,\tau} \right] \\ & + (1 - \lambda \cos(\omega)) \eta - b\eta^3 = \lambda \epsilon \cos(\omega) \end{aligned} \quad (2.23)$$

Dividing (2.23) through by $(1 - \lambda \cos(\omega))$ gives,

$$\begin{aligned} & \left[\eta_{,\hat{t}\hat{t}} + \frac{2}{1 - \lambda \cos(\omega)^{1/2}} (\mu'_1 \epsilon + \mu'_2 \epsilon^2 + \mu'_3 \epsilon^3 + \dots) \eta_{,\hat{t}\hat{t}} + \frac{1}{(1 - \lambda \cos(\omega))} (\mu'_1 \epsilon + \mu'_2 \epsilon^2 + \mu'_3 \epsilon^3 + \dots) \eta_{,\hat{t}\hat{t}} \right. \\ & + \frac{2\delta}{(1 - \lambda \cos(\omega))^{1/2}} \eta_{,\hat{t}\tau} + \frac{2\delta}{(1 - \lambda \cos(\omega))} (\mu'_1 \epsilon + \mu'_2 \epsilon^2 + \mu'_3 \epsilon^3 + \dots) \eta_{,\hat{t}\tau} \\ & \quad \left. + \frac{\lambda \delta \omega' \sin(\omega) \eta_{,\hat{t}}}{2(1 - \lambda \cos(\omega))^{3/2}} + \frac{\delta^2}{(1 - \lambda \cos(\omega))} \eta_{,\tau\tau} + \frac{1}{(1 - \lambda \cos(\omega))} (\mu''_1 \epsilon + \mu''_2 \epsilon^2 + \mu''_3 \epsilon^3 + \dots) \eta_{,\hat{t}} \right] \\ & + \left[\frac{2\delta}{(1 - \lambda \cos(\omega))^{1/2}} \eta_{,\hat{t}} + \frac{2\delta}{(1 - \lambda \cos(\omega))} (\mu'_1 \epsilon + \mu'_2 \epsilon^2 + \mu'_3 \epsilon^3 + \dots) \eta_{,\hat{t}} + \frac{2\delta^2}{(1 - \lambda \cos(\omega))} \eta_{,\tau} \right] \\ & + \eta - \frac{b}{(1 - \lambda \cos(\omega))} \eta^3 = \frac{\lambda \epsilon \cos(\omega)}{(1 - \lambda \cos(\omega))} \end{aligned} \quad (2.24)$$

Now it is pertinent to assume the following asymptotic series

$$\eta(\hat{t}, \tau) = \sum_{i=1}^{\infty} \sum_{j=0}^{\infty} \eta^{ij}(\hat{t}, \tau) \epsilon^i \delta^j \quad (2.25)$$

Where ij on η^{ij} indicates superscript but not powers

On expansion, (2.25) leads to,

$$\begin{aligned} \eta(\hat{t}, \tau) &= \epsilon (\eta^{10} + \delta \eta^{11} + \delta^2 \eta^{12} + \dots) + \epsilon^2 (\eta^{20} + \delta \eta^{21} + \delta^2 \eta^{22} + \dots) \\ &+ \epsilon^3 (\eta^{30} + \delta \eta^{31} + \delta^2 \eta^{32} + \dots) + \dots \end{aligned} \quad (2.25)$$

Equating equations of orders $(\epsilon^i \delta^j)$ in (2.24) using (2.25) and (2.26), gives the following equations,

$$O(\epsilon): \eta_{,\hat{t}\hat{t}}^{10} + \eta^{10} = \frac{\lambda \cos(\omega)}{1 - \lambda \cos(\omega)} \quad (2.27a)$$

$$O(\epsilon\delta): \eta_{\hat{t}\hat{t}}^{11} + \eta^{11} = \frac{-2\eta_{\hat{t}\hat{t}}^{10}}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{2\eta_{\hat{t}\hat{t}}^{10}}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{\lambda\omega' \sin(\omega)\eta_{\hat{t}}^{10}}{2(1 - \lambda \cos(\omega))^{3/2}} \quad (2.27b)$$

$$O(\epsilon\delta^2): \eta_{\hat{t}\hat{t}}^{12} + \eta^{12} = \frac{-2\eta_{,\tau}^{10}}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{\eta_{,\tau\tau}^{10}}{(1 - \lambda \cos(\omega))} - \frac{-2\eta_{,\hat{t}\tau}^{11}}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{2\eta_{\hat{t}}^{11}}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{\lambda\omega' \sin(\omega)\eta_{\hat{t}}^{11}}{2(1 - \lambda \cos(\omega))^{3/2}} \quad (2.27c)$$

$$O(\epsilon^3): \eta_{\hat{t}\hat{t}}^{30} + \eta^{30} = \frac{b(\eta^{10})^3}{(1 - \lambda \cos(\omega))} - \frac{2\mu_2' \eta_{\hat{t}\hat{t}}^{10}}{(1 - \lambda \cos(\omega))} \quad (2.27d)$$

$$O(\epsilon^3\delta): \eta_{\hat{t}\hat{t}}^{31} + \eta^{31} = \frac{3b(\eta^{10})^2\eta^{11}}{(1 - \lambda \cos(\omega))} - \frac{2\mu_2' \eta_{\hat{t}\hat{t}}^{11}}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{2\mu_2' \eta_{\hat{t}}^{30}}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{2\eta_{,\tau}^{30}}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{2\mu_2' \eta_{,\hat{t}\tau}^{10}}{(1 - \lambda \cos(\omega))} - \frac{2\mu_2' \eta_{,\hat{t}}^{10}}{(1 - \lambda \cos(\omega))} - \frac{\mu_2'' \eta_{,\hat{t}}^{11}}{(1 - \lambda \cos(\omega))} - \frac{\lambda\omega' \sin(\omega)\eta_{\hat{t}}^{30}}{2(1 - \lambda \cos(\omega))^{3/2}} \quad (2.27e)$$

$$O(\epsilon^3\delta^2): \eta_{\hat{t}\hat{t}}^{32} + \eta^{32} = \frac{3b}{(1 - \lambda \cos(\omega))} \{ \eta^{10}(\eta^{11})^2 + (\eta^{10})^2\eta^{12} \} - \frac{2\mu_2' \eta_{\hat{t}\hat{t}}^{12}}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{2\eta_{,\hat{t}\tau}^{31}}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{\eta_{,\hat{t}}^{31}}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{2\mu_2' \eta_{,\hat{t}\tau}^{11}}{(1 - \lambda \cos(\omega))} - \frac{2\mu_2' \eta_{,\hat{t}}^{11}}{(1 - \lambda \cos(\omega))} - \frac{\eta_{,\hat{t}}^{11}\eta_{,\hat{t}}^{11}}{(1 - \lambda \cos(\omega))} - \frac{2\eta_{,\tau}^{30}}{(1 - \lambda \cos(\omega))} - \frac{\eta_{,\tau\tau}^{30}}{(1 - \lambda \cos(\omega))} - \frac{\lambda\omega' \sin(\omega)\eta_{\hat{t}}^{31}}{2(1 - \lambda \cos(\omega))^{3/2}} \quad (2.27f)$$

The initial conditions are,

$$\eta(0) = \frac{d\eta(0)}{dt} = 0 \quad (2.28a)$$

However, realizing the fact that,

$$\frac{d\eta}{dt} = (1 - \lambda \cos(\omega))^{1/2} \eta_{,\hat{t}} + (\mu_2'(\tau)\epsilon^2 + \mu_3'(\tau)\epsilon^3 + \dots)\eta_{,\hat{t}} + \delta\eta_{,\tau} \quad (2.28b)$$

the velocity initial condition $\frac{d\eta}{dt} = 0$ in (2.28b) becomes,

$$\eta_{,\hat{t}} + (1 - \lambda \cos(\omega))^{-1/2} \{ \mu_2'\epsilon^2 + \mu_3'\epsilon^3 + \dots \} \eta_{,\hat{t}} + \delta(1 - \lambda \cos(\omega))^{-1/2} \eta_{,\tau} = 0 \quad (2.29)$$

Taking the initial conditions, (2.29) results to

$$\eta_{,\hat{t}}(0,0) + (1 - \lambda)^{-1/2} \{ \mu_2'\epsilon^2 + \mu_3'\epsilon^3 + \dots \} \eta_{,\hat{t}}(0,0) + \delta(1 - \lambda)^{-1/2} \eta_{,\tau}(0,0) = 0 \quad (2.30)$$

Other initial conditions in orders of $(\epsilon^i\delta^j)$ are,

$$\eta^{ij}(0,0) = 0 \quad \forall i, j \quad (2.31a)$$

$$O(\epsilon): \eta^{10}(0,0) = \eta_{\hat{t}}^{10}(0,0) = 0 \quad (2.31b)$$

$$O(\epsilon\delta): \eta_{\hat{t}}^{11}(0,0) + (1 - \lambda)^{-1/2} \eta_{,\tau}^{10} = 0 \quad (2.31c)$$

$$O(\epsilon\delta^2): \eta_{\hat{t}}^{12}(0,0) + (1 - \lambda)^{-1/2} \eta_{,\tau}^{11} = 0 \quad (2.31d)$$

$$O(\epsilon^3): \eta_{\hat{t}}^{30}(0,0) + (1 - \lambda)^{-1/2} \mu_2'(0)\eta_{\hat{t}}^{10} = 0 \quad (2.31e)$$

$$O(\epsilon^3\delta): \eta_{\hat{t}}^{31}(0,0) + (1 - \lambda)^{-1/2} \{ \mu_2'(0)\eta_{\hat{t}}^{11}(0,0) + \eta_{,\tau}^{30}(0,0) \} = 0 \quad (2.31f)$$

$$O(\epsilon^3\delta^2): \eta_{\hat{t}}^{32}(0,0) + (1 - \lambda)^{-1/2} \{ \mu_2'(0)\eta_{\hat{t}}^{12}(0,0) + \eta_{,\tau}^{31}(0,0) \} = 0 \quad (2.31g)$$

3.1 Solution of the equations of orders η^{ij} of the Model Problem

From equation (2.27a), we have

$$\eta_{\hat{t}\hat{t}}^{10} + \eta^{10} = \frac{\lambda \cos(\omega)}{(1 - \lambda \cos(\omega))} \quad (2.31b)$$

with initial conditions (2.31a) and

Solving (2.27a), results to,

$$\eta^{10}(\hat{t}, \tau) = a_{10}(\tau)\cos\hat{t} + b_{10}(\tau)\sin\hat{t} + B(\tau) \tag{3.1a}$$

where,

$$B(\tau) = \frac{\lambda\cos(\omega)}{(1-\lambda\cos(\omega))} \tag{3.1b}$$

Using the initial conditions (2.31a, b) in (2.32), gives

$$\eta^{10}(0,0) = a_{10}(0) + B(0) = 0$$

$$\therefore a_{10}(0) = -B(0) = -\frac{\lambda}{1-\lambda}$$

From (2.31b), it follows that,

$$\eta_{,\hat{t}}^{10}(0,0) = b_{10}(0) = 0$$

$$\therefore b_{10}(0) = 0$$

Next, solving (2.27b), gives,

$$\eta_{,\hat{t}\hat{t}}^{11} + \eta^{11} = \frac{-2}{(1-\lambda\cos(\omega))^{1/2}} \{ \eta_{,\hat{t}\tau}^{10} + \eta_{,\hat{t}}^{10} \} - \frac{\lambda\omega' \sin(\omega) \eta_{,\hat{t}}^{10}}{2(1-\lambda\cos(\omega))^{3/2}} \tag{3.2a}$$

with initial conditions,

$$\eta^{11}(0,0) = 0, \eta_{,\hat{t}}^{11}(0,0) + (1-\lambda)^{-1/2} \eta_{,\tau}(0,0) = 0.$$

Substituting for $\eta_{,\hat{t}}^{10}$ and $\eta_{,\hat{t}\tau}^{10}$ in (2.2a), gives,

$$\eta_{,\hat{t}\hat{t}}^{11} + \eta^{11} = \left\{ \frac{2(a'_{10} + a_{10})}{(1-\lambda\cos(\omega))^{1/2}} + \frac{a_{10}\lambda\omega' \sin(\omega)}{2(1-\lambda\cos(\omega))^{3/2}} \right\} \sin\hat{t} - \left\{ \frac{2(b'_{10} + b_{10})}{(1-\lambda\cos(\omega))^{1/2}} + \frac{2(b'_{10} + b_{10})}{(1-\lambda\cos(\omega))^{1/2}} \right\} \cos\hat{t} \tag{3.2b}$$

To ensure a uniformly valid asymptotic solution in \hat{t} , it is necessary to equate to zero the coefficients of $\sin\hat{t}$ and $\cos\hat{t}$ respectively in (3.2b).

Thus, it follows from the coefficients of $\sin\hat{t}$, that,

$$\frac{2(a'_{10} + a_{10})}{(1-\lambda\cos(\omega))^{1/2}} + \frac{a_{10}\lambda\omega' \sin(\omega)}{2(1-\lambda\cos(\omega))^{3/2}} = 0 \tag{3.2c}$$

and from the coefficient of $\cos\hat{t}$, the result is

$$\frac{2(b'_{10} + b_{10})}{(1-\lambda\cos(\omega))^{1/2}} + \frac{b_{10}\lambda\omega' \sin(\omega)}{2(1-\lambda\cos(\omega))^{3/2}} = 0 \tag{3.2d}$$

Solving (3.2c), gives,

$$\frac{a'_{10}}{a_{10}} + \frac{\lambda\omega' \sin(\omega)}{4(1-\lambda\cos(\omega))} = -1 \tag{3.2e}$$

Now integrating both sides (4.23e) with respect to τ , gives

$$\ln a_{10} + \frac{1}{4} \ln(1-\lambda\cos(\omega)) = -\tau + C_1$$

where C_1 is an arbitrary constant.

$$i.e \ln a_{10}(1-\lambda\cos(\omega))^{1/4} = -\tau + C_1, \therefore a_{10}(1-\lambda\cos(\omega))^{1/4} = e^{-\tau+C_1}$$

$$a_{10}(1-\lambda\cos(\omega))^{1/4} = A_0 e^{-\tau}, \therefore a_{10}(\tau) = \frac{A_0 e^{-\tau}}{(1-\lambda\cos(\omega))^{1/4}}, \text{ where } A_0 = e^{C_1} (\text{constant})$$

$$a_{10}(0)(1-\lambda)^{1/4} = A_0 = -B(0)(1-\lambda)^{1/4}, \therefore a_{10}(\tau) = -B(0)e^{-\tau} \left[\frac{1-\lambda}{(1-\lambda\cos(\omega))} \right]^{1/4}$$

Similarly, solving (3.2d), gives,

$$\frac{b'_{10}}{b_{10}} + \frac{\lambda\omega' \sin(\omega)}{4(1-\lambda\cos(\omega))} = -1 \tag{3.2f}$$

Integrating both sides of (3.2f) w.r. t τ , gives,

$$\ln b_{10} + \frac{1}{4} \ln(1-\lambda\cos(\omega)) = -\tau + C_2$$

where C_2 is an arbitrary constant.

$$i.e \ln b_{10}(1-\lambda\cos(\omega))^{1/4} = -\tau + C_2 \text{ and } b_{10}(\tau)(1-\lambda\cos(\omega))^{1/4} = e^{-\tau+C_2} = A_1 e^{-\tau}$$

where $A_1 = e^{C_2}$ and for $\tau = 0$

$$b_{10}(0)(1-\lambda)^{1/4} = A_1 = 0 \text{ and } b_{10}(\tau) = 0$$

Substituting $b_{10}(\tau)$ in (3.1), gives

$$\eta^{10}(\hat{t}, \tau) = a_{10}(\tau) \cos \hat{t} + B(\tau) \tag{3.3}$$

Furthermore, solving the remaining part of equation (3.2b) gives

$$\eta^{11}(\hat{t}, \tau) = a_{11}(\tau) \cos \hat{t} + b_{10}(\tau) \sin \hat{t} \tag{3.4a}$$

Then, applying the initial conditions in (2.31b), gives

$$\eta^{11}(0,0) = a_{11}(0) = 0, \therefore a_{11}(0) = 0$$

From $\eta_{,\hat{t}}^{11}(0,0) = b_{11}(0) = 0$, thus, $b_{11}(0) = 0$

Now solving (2.27c), gives

$$\eta_{,\hat{t}\hat{t}}^{12} + \eta^{12} = \frac{-2}{(1 - \lambda \cos(\omega))^{1/2}} \{ \eta_{,\hat{t}\tau}^{11} + \eta_{,\tau}^{11} \} - \frac{1}{(1 - \lambda \cos(\omega))^{1/2}} \{ \eta_{,\tau\tau}^{10} + 2\eta_{,\tau}^{10} \} - \frac{\lambda \omega' \sin(\omega) \eta_{,\hat{t}}^{11}}{2(1 - \lambda \cos(\omega))^{3/2}} \tag{3.4b}$$

with the initial conditions

$$\eta^{12}(0,0) = 0 \text{ and } \eta_{,\hat{t}}^{12}(0,0) + (1 - \lambda)^{-1/2} \eta_{,\tau}^{11} \tau(0,0) = 0 \tag{3.4c}$$

Substituting $\eta_{,\hat{t}}^{11}, \eta_{,\hat{t}\tau}^{11}, \eta_{,\tau}^{10}$ and $\eta_{,\tau\tau}^{10}$ in (2.27c), gives

$$\begin{aligned} \eta_{,\hat{t}\hat{t}}^{12} + \eta^{12} = & \left\{ \frac{2(a'_{11} + a_{11})}{(1 - \lambda \cos(\omega))^{1/2}} + \frac{a_{11} \lambda \omega' \sin(\omega)}{2(1 - \lambda \cos(\omega))^{3/2}} - \frac{(b''_{10} + 2b'_{10})}{(1 - \lambda \cos(\omega))} \right\} \sin \hat{t} \\ & - \left\{ 2 \left(\frac{b'_{11} + b_{11}}{(1 - \lambda \cos(\omega))^{1/2}} + \frac{b_{11} \lambda \omega' \sin(\omega)}{2(1 - \lambda \cos(\omega))^{3/2}} - \frac{(a''_{10} + 2a'_{10})}{(1 - \lambda \cos(\omega))} \right) \right\} \cos \hat{t} - \frac{(B''(\tau) + 2B'(\tau))}{(1 - \lambda \cos(\omega))} \end{aligned} \tag{3.5a}$$

To ensure a uniformly valid asymptotic solution in \hat{t} , there is need to equate to zero the coefficients of $\sin \hat{t}$ and $\cos \hat{t}$ respectively in (3.5a).

The coefficient of $\sin \hat{t}$, gives

$$\frac{2(a'_{11} + a_{11})}{(1 - \lambda \cos(\omega))^{1/2}} + \frac{a_{11} \lambda \omega' \sin(\omega)}{2(1 - \lambda \cos(\omega))^{3/2}} - \frac{(b''_{10} + 2b'_{10})}{(1 - \lambda \cos(\omega))} = 0 \tag{3.5b}$$

From the coefficient of $\cos \hat{t}$, the simplification gives

$$\frac{2(b'_{11} + b_{11})}{(1 - \lambda \cos(\omega))^{1/2}} + \frac{b_{11} \lambda \omega' \sin(\omega)}{2(1 - \lambda \cos(\omega))^{3/2}} - \frac{(a''_{10} + 2a'_{10})}{(1 - \lambda \cos(\omega))} = 0 \tag{3.5c}$$

Solving equation (3.5b), gives

$$\frac{2(a'_{11} + a_{11})}{(1 - \lambda \cos(\omega))^{1/2}} + \frac{a_{11} \lambda \omega' \sin(\omega)}{2(1 - \lambda \cos(\omega))^{3/2}} = 0 \tag{3.5d}$$

Because $b_{10}(\tau) = 0$, then, $b'_{10} = b''_{10} = 0$

$$i.e \quad \frac{a'_{11}}{a_{11}} + \frac{\lambda \omega' \sin(\omega)}{4(1 - \lambda \cos(\omega))} = -1 \tag{3.5e}$$

Integrating both sides of (3.5d) w.r.t. τ , gives

$$In a_{11} + \frac{1}{4} In(1 - \lambda \cos(\omega)) = -\tau + C_3$$

Where C_3 is an arbitrary constant.

$$i.e \quad In a_{11} (1 - \lambda \cos(\omega))^{1/4} = -\tau + C_3$$

$$a_{11}(\tau) (1 - \lambda \cos(\omega))^{1/4} = e^{-\tau + C_3} = A_3 e^{-\tau} \text{ (where } A_3 = e^{C_3} \text{)}$$

$$a_{11}(0) (1 - \lambda)^{1/4} = A_3 = 0, \therefore a_{11}(\tau) = 0$$

Similarly, solving (3.5c), gives

$$\frac{2(b'_{11} + b_{11})}{(1 - \lambda \cos(\omega))^{1/2}} + \frac{b_{11} \lambda \omega' \sin(\omega)}{2(1 - \lambda \cos(\omega))^{3/2}} = \frac{(a''_{10} + 2a'_{10})}{(1 - \lambda \cos(\omega))} \tag{3.5f}$$

$$i.e \quad b'_{11} + b_{11} \left\{ 1 + \frac{\lambda \omega' \sin(\omega)}{4(1 - \lambda \cos(\omega))} \right\} = \frac{(a''_{10} + 2a'_{10})}{2(1 - \lambda \cos(\omega))} \tag{3.5g}$$

Integrating both sides of (3.5g) gives,

$$b_{11}(\tau) e^{\tau}(1 - \lambda \cos(\omega))^{1/4} = \left[\int_0^{\tau} \frac{e^s(a_{10}'' + 2a_{10}')ds}{2(1 - \lambda \cos(\omega))^{1/4}} + C_4 \right] \quad (3.5I)$$

$$b_{11}(0) = (1 - \lambda)^{-1/4}[0 + C_4] = C_4(1 - \lambda)^{-1/4} = 0, \tau = 0, \therefore C_4 = 0$$

Hence,

$$b_{11}(\tau) = e^{-\tau}(1 - \lambda \cos(\omega))^{-1/4} \left[\int_0^{\tau} \frac{e^s(a_{10}'' + 2a_{10}')ds}{2(1 - \lambda \cos(\omega))^{1/2}} \right] \\ \therefore \eta^{11}(\hat{t}, \tau) = b_{11}(\tau) \sin \hat{t}; \text{ (because } a_{11}(\tau) = 0 \text{)} \quad (3.6)$$

There remaining part of equation (3.5a) is

$$\eta_{,\hat{t}\hat{t}}^{12} + \eta^{12} = - \left(\frac{B''(\tau) + 2B'(\tau)}{(1 - \lambda \cos(\omega))} \right) \quad (3.7a)$$

Solving (3.7a), the result gives

$$\eta^{12}(t, \tau) = a_{12}(\tau) \cos \hat{t} + b_{12}(\tau) \sin \hat{t} - \left(\frac{B''(\tau) + 2B'(\tau)}{(1 - \lambda \cos(\omega))} \right) \quad (3.7b)$$

Applying the initial conditions (2.31a) and (2.31d) in (3.7b), gives

$$\eta^{12}(0,0) = a_{12}(0) - \frac{B''(0)}{(1 - \lambda)} = 0; \text{ because } B'(0) = 0 \\ \therefore a_{12}(0) = \frac{B''(0)}{(1 - \lambda)} = \frac{B(0)\omega'^2(0)(2\lambda - 1)}{(1 - \lambda)^2} \text{ and } b_{12}(0) = 0 \quad (3.7c)$$

3.2 Solution of the equations of orders $\eta^{3j}, j = 0, 1, 2$ of the model problem

The next solution contains terms such as $(\eta^{10})^3$ which need to be evaluated before substitution.

Doing this, the following is obtained

$$(\eta^{10})^3 = (a_{10} \cos \hat{t} + B)^3 = \left(B^3 + \frac{3a_{10}^2 B}{2} \right) + \left(\frac{3a_{10}^3}{4} + 3a_{10} B^2 \right) \cos \hat{t} \\ + \frac{3}{2} a_{10}^2 \cos 2\hat{t} + \frac{a_{10}^3}{4} \cos 3\hat{t} \quad (3.8)$$

Substituting (3.8) in (2.28d), gives

$$\eta_{,\hat{t}\hat{t}}^{30} + \eta^{30} = \frac{3b}{(1 - \lambda \cos(\omega))} \left[\left(B^3 + \frac{3a_{10}^2 B}{2} \right) + \left(\frac{3a_{10}^3}{4} + 3a_{10} B^2 \right) \cos \hat{t} + \frac{3}{2} a_{10}^2 \cos 2\hat{t} + \frac{a_{10}^3}{4} \cos 3\hat{t} \right] \\ + \frac{2\mu_2' a_{10} \cos \hat{t}}{(1 - \lambda \cos(\omega))^{1/2}} \quad (3.9)$$

with initial conditions,

$$\eta^{30}(0,0) = 0; \eta_{,\hat{t}}^{30}(0,0) + (1 - \lambda)^{1/2} [\mu_2'(0) \eta_{,\hat{t}}^{10}(0,0)] = 0$$

Ensuring a uniformly valid asymptotic solution in \hat{t} , needs equating to zero the coefficients of $\sin \hat{t}$ and $\cos \hat{t}$ respectively in (3.9).

Thus, the coefficient of $\cos \hat{t}$, gives

$$\frac{3b}{(1 - \lambda \cos(\omega))} \left\{ \frac{a_{10}^3}{4} + a_{10} B^2 \right\} + \frac{2\mu_2' a_{10}}{(1 - \lambda \cos(\omega))^{1/2}} = 0 \quad (3.10)$$

From (3.10), it follows that

$$\mu_2' = \frac{-3b(a_{10}^2 + 4B^2)}{8(1 - \lambda \cos(\omega))^{1/2}} \quad (3.11)$$

The remaining equation (3.9) is

$$\eta_{,\hat{t}\hat{t}}^{30} + \eta^{30} = \frac{b}{(1 - \lambda \cos(\omega))} \left[\left(\frac{3}{2} a_{10}^2 B + B^3 \right) + \frac{3}{2} a_{10}^2 B \cos 2\hat{t} + \frac{3}{4} a_{10}^3 \cos 3\hat{t} \right] \quad (3.12a)$$

The solution (3.12a) is

$$\eta^{30}(\hat{t}, \tau) = a_{30}(\tau)\cos\hat{t} + b_{30}(\tau)\sin\hat{t} + \frac{b}{(1 - \lambda\cos(\omega))} \left[\left(\frac{3a_{10}^2 B}{2} + B^3 \right) - \frac{Ba_{10}^2}{2}\cos 2\hat{t} - \frac{3a_{10}^3 \cos 3\hat{t}}{32} \right] \quad (3.12b)$$

$$\eta^{30}(\hat{t}, \tau) = a_{30}(\tau)\cos\hat{t} + b_{30}(\tau)\sin\hat{t} + b[S_0(\tau) + S_1(\tau)\cos 2\hat{t} + S_2(\tau)\cos 3\hat{t}] \quad (3.12c)$$

where,

$$S_0(\tau) = \frac{1}{(1 - \lambda\cos(\omega))} \left(\frac{3}{2}Ba_{10}^2 + B^3 \right) \quad (3.12d)$$

$$S_1(\tau) = \frac{-Ba_{10}^2}{2(1 - \lambda\cos(\omega))} ; S_2(\tau) = \frac{-3a_{10}^3}{32(1 - \lambda\cos(\omega))} \quad (3.12e)$$

and where,

$$S_0(0) = \frac{5B^3(0)}{2(1 - \lambda)} ; S_1(0) = \frac{-B^3(0)}{2(1 - \lambda)} ; S_2(0) = \frac{3B^3(0)}{32(1 - \lambda)} \quad (3.12f)$$

Using the initial conditions in (3.12c), gives

$$\begin{aligned} \eta^{30}(0,0) &= a_{30}(0) + b[S_0(0) + S_1(0) + S_2(0)] = 0 \\ \therefore a_{30}(0) &= -b \left[\frac{5B^3(0)}{2(1 - \lambda)} - \frac{B^3(0)}{2(1 - \lambda)} + \frac{3B^3(0)}{32(1 - \lambda)} \right] = -\frac{67bB^3(0)}{32(1 - \lambda)} ; b_{30}(0) = 0 \end{aligned} \quad (3.12g)$$

In the next solution, there shall be the need for terms like $B'(0), S'_0(0), S'_1(0)$ and $S'_2(0)$ which are necessary and are evaluated as follows

$$\begin{aligned} B'(\tau) &= (1 - \lambda\cos(\omega)) \left[\frac{-\lambda\omega' \sin(\omega) - \lambda^2\omega' \sin(\omega)\cos(\omega)}{(1 - \lambda\cos(\omega))^2} \right] ; \therefore B'(0) = 0 \\ S'_0(\tau) &= \frac{1}{(1 - \lambda\cos(\omega))} \left[\frac{3}{2}(2Ba_{10}a'_{10} + B'a_{10}^2 + 3B^2B) + \left(\frac{3Ba_{10}^2}{2} + B^3 \right) \left(\frac{-\lambda\omega' \sin(\omega)}{(1 - \lambda\cos(\omega))^2} \right) \right], S'_0(0) = 0 \\ S'_1(\tau) &= -\frac{1}{2} \left[\left(\frac{B'a_{10}^2 + 2Ba_{10}a'_{10}}{(1 - \lambda\cos(\omega))} \right) + \left(\frac{Ba_{10}^2\lambda\omega' \sin(\omega)}{(1 - \lambda\cos(\omega))^2} \right) \right], S'_1(0) = 0 \\ S'_2(\tau) &= \frac{-3}{32} \left[\frac{3a'_{10}a_{10}^2}{(1 - \lambda\cos(\omega))} - \frac{a_{10}^3\lambda\omega' \sin(\omega)}{(1 - \lambda\cos(\omega))^2} \right], S'_2(0) = 0 \end{aligned}$$

The following equation is obtained on substituting in (2.27e)

$$\begin{aligned} \eta_{\hat{t}\hat{t}}^{31} + \eta^{31} &= \frac{3b(\eta^{10})^2\eta^{11}}{(1 - \lambda\cos(\omega))} - \frac{2\mu'_2\eta_{\hat{t}\hat{t}}^{11}}{(1 - \lambda\cos(\omega))^{1/2}} - \frac{2\eta_{\hat{t}}^{30}}{(1 - \lambda\cos(\omega))^{1/2}} - \frac{2\eta_{\hat{t}\tau}^{30}}{(1 - \lambda\cos(\omega))^{1/2}} - \frac{2\mu'_2\eta_{\hat{t}\tau}^{10}}{(1 - \lambda\cos(\omega))} \\ &\quad - \frac{\mu''_2\eta_{\hat{t}}^{10}}{(1 - \lambda\cos(\omega))} - \frac{2\mu'_2\eta^{10}}{(1 - \lambda\cos(\omega))} - \frac{\lambda\omega' \sin(\omega)\eta_{\hat{t}}^{30}}{2(1 - \lambda\cos(\omega))^{3/2}} \end{aligned} \quad (3.13)$$

with initial conditions,

$$\eta^{31}(0,0) = 0 \text{ and } \eta_{\hat{t}}^{31}(0,0) + (1 - \lambda)^{1/2} [\mu'_2(0)\eta_{\hat{t}}^{11}(0,0) + \eta_{\tau}^{30}(0,0)] = 0$$

Next, it is necessary to evaluate the term $(\eta^{10})^2\eta^{11}$ first, before going forward

The following is obtained in this case,

$$(\eta^{10})^2\eta^{11} = b_{11} \left(\frac{a_{10}^2}{4} + B \right) \sin\hat{t} + b_{11}Ba_{10}\sin 2\hat{t} + \frac{b_{11}a_{10}^2\sin 3\hat{t}}{4} \quad (3.14)$$

Substituting (3.14) in (3.13), gives

$$\begin{aligned} \eta_{\hat{t}\hat{t}}^{31} + \eta^{31} &= \frac{3b}{(1 - \lambda\cos(\omega))} \left[b_{11} \left(\frac{a_{10}^2}{4} + B^2 \right) \sin\hat{t} + b_{11}Ba_{10}\sin 2\hat{t} + \frac{b_{11}a_{10}^2\sin 3\hat{t}}{4} \right] + \frac{2\mu'_2b_{11}\sin\hat{t}}{(1 - \lambda\cos(\omega))^{1/2}} \\ &\quad - \frac{2}{(1 - \lambda\cos(\omega))^{1/2}} \{ (-a_{30}\sin\hat{t} + b_{30}\cos\hat{t}) + b(-2S_1\sin 2\hat{t} - 3S_2\sin 3\hat{t}) \} \end{aligned}$$

$$\begin{aligned} & \frac{-2}{(1-\lambda \cos(\omega))^{1/2}} [-a'_{30} \sin \hat{t} + b'_{30} \cos \hat{t} + b(-2S'_1 \sin 2\hat{t} - 3S'_2 \sin 3\hat{t})] + \frac{2\mu'_2 a'_{10} \sin \hat{t}}{(1-\lambda \cos(\omega))} \\ & + \frac{\mu''_2 a_{10} \sin \hat{t}}{(1-\lambda \cos(\omega))} + \frac{2\mu'_2 a_{10} \sin \hat{t}}{(1-\lambda \cos(\omega))} - \frac{\lambda \omega' \sin(\omega)}{2(1-\lambda \cos(\omega))^{3/2}} \{-a_{30} \sin \hat{t} + b_{30} \cos \hat{t} \\ & + b(-2S_1 \sin 2\hat{t} - 3S_2 \sin 3\hat{t})\} \end{aligned} \quad (3.15)$$

To ensure a uniformly valid asymptotic solution in \hat{t} , it necessary to equate to zero the coefficients of $\sin \hat{t}$ and $\cos \hat{t}$ respectively in (3.15).

From the coefficient of $\sin \hat{t}$, the resultant equation is

$$\begin{aligned} & \frac{3bb_{11}}{4(1-\lambda \cos(\omega))} (a_{10}^2 + 4B^2) + \frac{2\mu'_2 b_{11}}{(1-\lambda \cos(\omega))^{1/2}} + \frac{2a_{30}}{(1-\lambda \cos(\omega))^{1/2}} + \frac{2a'_{30}}{(1-\lambda \cos(\omega))^{1/2}} \\ & + \frac{2\mu'_2 a'_{10}}{(1-\lambda \cos(\omega))} + \frac{\mu''_2 a_{10}}{(1-\lambda \cos(\omega))} + \frac{2\mu'_2 a_{10}}{(1-\lambda \cos(\omega))} + \frac{a_{30} \lambda \omega' \sin(\omega)}{2(1-\lambda \cos(\omega))^{3/2}} = 0 \end{aligned} \quad (3.16a)$$

For the coefficient of $\cos \hat{t}$, it easily follows that

$$\frac{2b'_{30}}{(1-\lambda \cos(\omega))^{1/2}} + \frac{2b_{30}}{(1-\lambda \cos(\omega))^{1/2}} + \frac{b_{30} \lambda \omega' \sin(\omega)}{2(1-\lambda \cos(\omega))^{3/2}} = 0 \quad (3.16b)$$

A rearrangement of (3.16a) gives

$$\begin{aligned} & \frac{2a'_{30}}{(1-\lambda \cos(\omega))^{1/2}} + \frac{2a_{30}}{(1-\lambda \cos(\omega))^{1/2}} + \frac{a_{30} \lambda \omega' \sin(\omega)}{2(1-\lambda \cos(\omega))^{3/2}} \\ & = - \left[\frac{3bb_{11}}{4(1-\lambda \cos(\omega))} (a_{10}^2 + B^2) + \frac{2\mu'_2 b_{11}}{(1-\lambda \cos(\omega))^{1/2}} \right. \\ & \left. + \frac{2\mu'_2 a'_{10}}{(1-\lambda \cos(\omega))} + \frac{2\mu'_2 a_{10}}{(1-\lambda \cos(\omega))} + \frac{\mu''_2 a_{10}}{(1-\lambda \cos(\omega))} \right] \\ & \text{i.e. } a'_{30} + a_{30} \left(1 + \frac{\lambda \omega' \sin(\omega)}{4(1-\lambda \cos(\omega))} \right) = q_1(\tau) \end{aligned} \quad (3.16c)$$

where,

$$q_1(\tau) = - \left(\frac{1-\lambda \cos(\omega)}{2} \right)^{1/2} \left[\frac{3bb_{11}}{(1-\lambda \cos(\omega))^{1/2}} (a_{10}^2 + B^2) + \frac{2\mu'_2 b_{11}}{(1-\lambda \cos(\omega))^{1/2}} + \frac{2\mu'_2 a'_{10}}{(1-\lambda \cos(\omega))} + \frac{\mu''_2 a_{10}}{(1-\lambda \cos(\omega))} + \frac{2\mu'_2 a_{10}}{(1-\lambda \cos(\omega))^{1/2}} \right] \quad (3.16d)$$

Solving (3.16c) gives,

$$\begin{aligned} \therefore a_{30}(\tau) &= e^{-\tau} (1-\lambda \cos(\omega))^{-1/4} \left[\int_0^\tau q_1(s) e^s (1-\lambda \cos \omega)^{1/4} + C_5 \right] \\ a_{30}(0) &= (1-\lambda)^{-1/4} [0 + C_5]; C_5 = \frac{67bB^3(0)}{32(1-\lambda)^{3/4}}; \left(\text{because } a_{30}(0) = -\frac{67bB^3(0)}{32(1-\lambda)} \right) \end{aligned}$$

Similarly, solving (3.16b) gives,

$$b'_{30} + b_{30} \left(1 + \frac{\lambda \omega' \sin(\omega)}{4(1-\lambda \cos(\omega))} \right) = 0 \quad (3.16f)$$

Solving (3.16f) gives,

$$b_{30} (1-\lambda \cos(\omega))^{1/4} e^\tau = C_6; \therefore b_{30}(\tau) = C_6 (1-\lambda \cos(\omega))^{-1/4} e^{-\tau}; b_{30}(0) = 0; \therefore C_6 = 0$$

Hence,

$$b_{30}(\tau) = 0$$

Substituting $b_{30}(\tau)$ in (3.12c), gives

$$\eta^{30}(\hat{t}, \tau) = a_{30}(\tau) \cos \hat{t} + b [S_0(\tau) + S_1(\tau) \cos 2\hat{t} + S_2(\tau) \cos 3\hat{t}] \quad (3.16h)$$

The remaining part of equation (3.15) is solved to get

$$\eta^{31}(\hat{t}, \tau) = a_{31}(\tau) \cos \hat{t} + b_{31}(\tau) \sin \hat{t} - \frac{S_3}{3} \sin 2\hat{t} - \frac{S_4 \sin 3\hat{t}}{8} \quad (3.16i)$$

where,

$$S_3(\tau) = \frac{3bb_{11}Ba_{10}}{(1 - \lambda \cos(\omega))} + \frac{bS_1\lambda\omega' \sin(\omega)}{2(1 - \lambda \cos(\omega))^{3/2}} + \frac{4bS_1}{(1 - \lambda \cos\omega)^{1/2}} + \frac{4bS'_1}{(1 - \lambda \cos\omega)^{1/2}} \quad (3.17a)$$

$$S_4(\tau) = \frac{3bb_{11}a_{10}^2}{4(1 - \lambda \cos(\omega))} + \frac{3bS_2\lambda\omega' \sin(\omega)}{2(1 - \lambda \cos(\omega))^{3/2}} + \frac{6bS_2}{(1 - \lambda \cos\omega)^{1/2}} + \frac{6bS'_2}{(1 - \lambda \cos\omega)^{1/2}} \quad (3.17b)$$

$$S_3(0) = \frac{20bB^3(0)}{(1 - \lambda)^{1/2}} = bB^3(0)S_5; S_5 = \frac{20}{(1 - \lambda)^{1/2}}; S_4(0) = \frac{-18bB^3(0)}{32(1 - \lambda)^{1/2}} = bB^3(0)S_6; S_6 = \frac{-18}{32(1 - \lambda)^{1/2}}$$

Using the initial condition, $\eta^{31}(0,0) = 0$ in (3.16h), gives,

$$\eta^{31}(0,0) = a_{31}(0) = 0; \therefore a_{31}(0) = 0$$

Using the second initial condition (2.31f) in (3.16h), gives

$$b_{31}(0) - \frac{2}{3}S_2(0) - \frac{3}{8}S_3(0) + (1 - \lambda)^{-1/2}[a_{30}(0) + b(S'_0(0) + S'_1(0) + S'_2(0))] = 0$$

$\therefore b_{31}(0) = 0$; (because $S'_0(0) = S'_1(0) = S'_2(0) = 0$)

Solving the equation (3.27f) gives

$$\begin{aligned} \eta_{,\hat{t}\hat{t}}^{32} + \eta^{32} &= \frac{3b}{(1 - \lambda \cos(\omega))} [\eta^{10}(\eta^{11})^2 + (\eta^{10})^2\eta^{12}] - \frac{\lambda\omega' \sin(\omega) \eta_{,\hat{t}}^{31}}{2(1 - \lambda \cos(\omega))^{3/2}} - \frac{2\eta_{,\hat{t}\hat{\tau}}^{31}}{(1 - \lambda \cos(\omega))^{1/2}} \\ &- \frac{2\eta_{,\hat{t}}^{31}}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{2\mu'_2 \eta_{,\hat{t}\hat{t}}^{12}}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{2\mu'_2 \eta_{,\hat{t}\hat{\tau}}^{11}}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{2\mu'_2 \eta_{,\hat{t}}^{11}}{(1 - \lambda \cos(\omega))} - \frac{\eta_{,\hat{\tau}\hat{\tau}}^{30}}{(1 - \lambda \cos(\omega))} \end{aligned} \quad (3.18a)$$

with the initial conditions,

$$\eta^{32}(0,0) = 0 \text{ and } \eta_{,\hat{t}}^{32}(0,0) + (1 - \lambda)^{-1/2}[\mu'_2(0)\eta_{,\hat{t}}^{12}(0,0) + \eta_{,\hat{\tau}}^{31}(0,0)] = 0$$

We need to evaluate $\eta^{10}(\eta^{11})^2 + (\eta^{10})^2\eta^{12}$ first before proceeding and obtain

$$\begin{aligned} \eta^{10}(\eta^{11})^2 + (\eta^{10})^2\eta^{12} &= \left[2Ba_{10}a_{12} - \frac{B''}{(1 - \lambda \cos\omega)} \left(\frac{a_{10}^2}{2} + B^2 \right) + \frac{Bb_{11}^2}{2} \right] + \left[a_{12} \left(\frac{a_{10}^2 + 2B^2}{2} \right) \right. \\ &- \left. \frac{2BB''a_{10}^2}{(1 - \lambda \cos\omega)} + \frac{a_{10}^2}{4} + \frac{b_{11}^2 a_{10}}{4} \right] \cos\hat{t} + \left[2Ba_{12}a_{10} - \frac{B''a_{10}^2}{(1 - \lambda \cos\omega)} - \frac{Bb_{11}^2}{2} \right] \cos 2\hat{t} \\ &+ \left[\frac{a_{12}a_{10}^2}{4} - \frac{b_{11}^2 a_{10}}{4} \right] \cos\hat{t} \end{aligned} \quad (3.18b)$$

Substituting (3.18b) in (3.18a) gives

$$\begin{aligned} \eta_{,\hat{t}\hat{t}}^{32} + \eta^{32} &= \frac{3b}{(1 - \lambda \cos\omega)} \left[\left\{ \left(2Ba_{10}a_{12} - \frac{B''}{(1 - \lambda \cos(\omega))} \left(\frac{a_{10}^2 + 2B^2}{2} \right) + Bb_{11}^2 \right) + \left\{ a_{12} \left(\frac{a_{10}^2 + 2B^2}{2} \right) \right. \right. \right. \\ &- \left. \left. \frac{2BB''a_{10}^2}{(1 - \lambda \cos(\omega))} + \frac{a_{10}^2}{4} + \frac{b_{11}^2 a_{10}}{4} \right\} \cos\hat{t} \right] + \left\{ \left\{ 2Ba_{12}a_{10} - \frac{B''a_{10}^2}{(1 - \lambda \cos(\omega))} - \frac{Bb_{11}^2}{2} \right\} \cos 2\hat{t} \right. \\ &+ \left. \left\{ \left(\frac{a_{12}a_{10}^2}{4} - \frac{b_{11}^2 a_{10}}{4} \right) \right\} \cos\hat{t} - \frac{\lambda\omega' \sin(\omega)}{2(1 - \lambda \cos(\omega))^{3/2}} \left\{ -a_{31}\sin\hat{t} + b_{31}\cos\hat{t} - \frac{2}{3}S_3\cos 2\hat{t} - \frac{3}{8}S_4\sin 3\hat{t} \right\} \right. \\ &- \frac{2}{(1 - \lambda \cos(\omega))^{1/2}} \left\{ -a'_{31}\sin\hat{t} + b'_{31}\cos\hat{t} - 2S'_3\cos 2\hat{t} + 3S'_4\cos 3\hat{t} \right\} - \frac{2}{(1 - \lambda \cos(\omega))^{1/2}} \left\{ -a_{31}\sin\hat{t} \right. \\ &+ \left. b_{31}\cos\hat{t} + 2S_3\cos 2\hat{t} + 3S_4\cos 3\hat{t} \right\} - \frac{2\mu'_2}{(1 - \lambda \cos(\omega))^{1/2}} \left\{ -a_{12}\cos\hat{t} - b_{12}\sin\hat{t} \right\} - \frac{2\mu'_2 b_{11}\cos\hat{t}}{(1 - \lambda \cos(\omega))^{1/2}} \\ &- \frac{\mu''_2 b_{11}\cos\hat{t}}{(1 - \lambda \cos(\omega))} - \frac{2}{(1 - \lambda \cos\omega)} \left\{ a'_{30}\sin\hat{t} + b'_{30}\cos\hat{t} + b(S'_0 + S'_1\cos 2\hat{t} + S'_2\cos 3\hat{t}) \right\} \end{aligned} \quad (3.19a)$$

Ensuring a uniformly valid asymptotic solution in \hat{t} is achieved by equating to zero the coefficients of $\cos\hat{t}$ and $\sin\hat{t}$ respectively in (3.19a).

From the coefficient of $\cos\hat{t}$, the resultant equation is

$$\begin{aligned} & \frac{3b}{(1-\lambda\cos(\omega))} \left[a_{12} \left(\frac{a_{10}^2 + 2B^2}{2} \right) - \frac{2BB''a_{10}^2}{(1-\lambda\cos(\omega))} + \frac{a_{10}^2}{4} + \frac{b_{11}^2 a_{10}}{4} \right] - \frac{b_{31}\lambda\omega'\sin(\omega)}{(1-\lambda\cos(\omega))^{3/2}} - \frac{2b'_{31}}{(1-\lambda\cos(\omega))^{1/2}} \\ & - \frac{2b_{31}}{(1-\lambda\cos(\omega))^{1/2}} + \frac{2\mu'_2 a_{12}}{(1-\lambda\cos(\omega))^{1/2}} - \frac{2\mu'_2 b'_{11}}{(1-\lambda\cos(\omega))^{1/2}} - \frac{2\mu'_2 b_{11}}{(1-\lambda\cos(\omega))} - \frac{2b'_{30}}{(1-\lambda\cos(\omega))} \\ & - \frac{\mu'_2 b_{11}}{(1-\lambda\cos(\omega))} - \frac{a''_{30}}{(1-\lambda\cos(\omega))} - \frac{b'_{30}}{(1-\lambda\cos(\omega))} - \frac{\mu'_2 b_{11}}{(1-\lambda\cos(\omega))} = 0 \end{aligned} \quad (3.19b)$$

From the coefficient of $\sin\hat{t}$, it follows that

$$\frac{a_{31}\lambda\omega'\sin(\omega)}{2(1-\lambda\cos(\omega))^{3/2}} + \frac{2a'_{31}}{(1-\lambda\cos(\omega))^{1/2}} + \frac{2a_{31}}{(1-\lambda\cos(\omega))^{1/2}} + \frac{2\mu'_2 b_{12}}{(1-\lambda\cos(\omega))^{1/2}} - \frac{2a'_{30}}{(1-\lambda\cos(\omega))} = 0 \quad (3.19c)$$

A re_arrangement of equation (3.19b) gives

$$b'_{31} + b_{31} \left(1 + \frac{\lambda\omega'\sin(\omega)}{4(1-\lambda\cos(\omega))} \right) = q_3(\tau) \quad (4.19d)$$

where,

$$\begin{aligned} q_3(\tau) & \left(\frac{1-\lambda\cos\omega}{2} \right)^{1/2} \left[\frac{3b}{(1-\lambda\cos(\omega))} \left\{ a_{12} \left(\frac{a_{10}^2 + 2B^2}{2} \right) - \frac{2BB''a_{10}^2}{(1-\lambda\cos(\omega))} + \frac{a_{10}^2}{4} + \frac{b_{11}^2 a_{10}}{4} \right\} + \frac{2\mu'_2 a_{12}}{(1-\lambda\cos(\omega))^{1/2}} \right. \\ & - \left. \frac{2\mu'_2 b'_{11}}{(1-\lambda\cos(\omega))^{1/2}} - \frac{2\mu'_2 b_{11}}{(1-\lambda\cos(\omega))} - \frac{a'_{30}}{(1-\lambda\cos\omega)} - \frac{2b'_{30}}{(1-\lambda\cos\omega)} \right. \\ & \left. - \frac{\mu''_2 b_{11}}{(1-\lambda\cos(\omega))} \right] \end{aligned}$$

Solving (3.19d), gives,

$$\begin{aligned} b_{31}(\tau)e^\tau(1-\lambda\cos(\omega))^{1/4} & = \left[\int_0^\tau q_3(s)e^s(1-\lambda\cos(\omega))^{1/4}ds + C_7 \right] \\ \therefore b_{31}(\tau) & = e^{-\tau}(1-\lambda\cos(\omega))^{-1/4} \left[\int_0^\tau \rho_3(s)e^s(1-\lambda\cos(\omega))^{1/4}ds + C_7 \right] \\ b_{31}(0) & = (1-\lambda)^{-1/4}[0 + C_7] = 0; \therefore C_7 = 0; \text{(because } b_{31}(0) = 0) \end{aligned}$$

Then, It follows that

$$b_{31}(\tau) = e^{-\tau}(1-\lambda\cos(\omega))^{-1/4} \left[\int_0^\tau \rho_3(s)e^s(1-\lambda\cos(\omega))^{1/4}ds \right] \quad (3.19f)$$

Solving (3.19c) gives

$$a'_{31} + a_{31} \left(1 + \frac{\lambda\omega'\sin(\omega)}{4(1-\lambda\cos(\omega))} \right) = \rho_4(\tau) \quad (3.20a)$$

where,

$$\rho_4(\tau) = \left(\frac{1-\lambda\cos(\omega)}{2} \right)^{1/2} \left[\frac{a'_{30}}{(1-\lambda\cos(\omega))} - \frac{2\mu'_2 b_{12}}{(1-\lambda\cos(\omega))^{1/2}} \right]$$

Solving (3.20a), gives,

$$\begin{aligned} a_{30}(\tau)e^\tau(1-\lambda\cos(\omega))^{1/4} & = \left[\int_0^\tau \rho_4(\tau)e^s(1-\lambda\cos(\omega))^{1/4}ds + C_8 \right] \\ a_{31}(0) & = (1-\lambda)^{-1/4}[0 + C_8] = 0 \therefore C_8 = 0; \text{(since } a_{31}(0) = 0) \end{aligned}$$

Then, it follows that,

$$a_{31}(\tau) = e^{-\tau}(1-\lambda\cos(\omega))^{-1/4} \left[\int_0^\tau \rho_4(s)e^s(1-\lambda\cos(\omega))^{1/4}ds \right] \quad (3.20b)$$

The remaining part of the equation (3.20a) is

$$\eta_{,\hat{t}\hat{t}}^{32} + \eta^{32} = S_7(\tau) + S_8(\tau)\cos 2\hat{t} + S_9(\tau)\sin 2\hat{t} + S_{10}(\tau)\cos 3\hat{t} + S_{11}(\tau)\sin 3\hat{t} \quad (3.21)$$

where;

$$S_7(\tau) = \frac{3b}{(1 - \lambda \cos \omega)} \left[2B a_{10} a_{12} - \frac{B''}{(1 - \lambda \cos(\omega))} \left(\frac{a_{10}^2 + 2B^2}{2} \right) + \frac{B b_{11}^2}{2} - \frac{2b s_0'}{(1 - \lambda \cos \omega)} \right] \quad (3.22a)$$

$$S_8(\tau) = \frac{3b}{(1 - \lambda \cos(\omega))} \left[2B a_{12} a_{10} - \frac{B'' a_{10}^2}{(1 - \lambda \cos(\omega))} - \frac{B b_{11}^2}{2} \right] - \frac{2S_3 \lambda \omega' \sin(\omega)}{6(1 - \lambda \cos(\omega))^{3/2}} + \frac{4S_3'}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{4S_3}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{2S_1'}{(1 - \lambda \cos(\omega))} \quad (3.22b)$$

$$S_9(\tau) = \frac{2S_1'(\tau)}{(1 - \lambda \cos(\omega))} \quad (3.22c)$$

$$S_{10}(\tau) = \left(\frac{a_{10}^2 a_{12} - b_{11}^2 a_{10}}{4} \right) + \frac{6S_4'}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{6S_4}{(1 - \lambda \cos(\omega))^{1/2}} - \frac{S_2'}{(1 - \lambda \cos(\omega))} \quad (3.22d)$$

$$S_{11}(\tau) = \frac{3S_2'}{(1 - \lambda \cos(\omega))} \quad (3.22e)$$

But,

$$S_7(0) = -3bB^2(0)S_{12}; S_{12} = \left\{ \frac{6\omega'^2(0) + B(0)(1 - \lambda)}{2(1 - \lambda)^2} \right\}; S_8(0) = 3b B(0)S_{13} \quad (3.23a, b)$$

where,

$$S_{13} = \left[\left\{ \frac{-4B''(0) - 2B(0)B''(0) - B^2(0)(1 - \lambda)}{2(1 - \lambda)^2} \right\} + \frac{4bB^2(0)S_{12}}{(1 - \lambda)^{1/2}} - \frac{4bB^2(0)S_5}{(1 - \lambda)^{1/2}} \right]$$

$$S_9(0) = S_{11}(0) = 0, S_{10}(0) = b^2 B S_{14} \quad (3.23c)$$

$$\text{where } S_{14} = \left[\left\{ \frac{B''(0) + B(0)(1 - \lambda)}{4(1 - \lambda)} \right\} + \frac{6bB(0)S_{13}}{(1 - \lambda)^{1/2}} - \frac{6bB(0)S_6}{(1 - \lambda)^{1/2}} \right]$$

The solution of (3.21) is

$$\eta^{32}(\hat{t}, \tau) = a_{32}(\tau)\cos \hat{t} + b_{32}(\tau)\sin \hat{t} + S_7(\tau) - \frac{S_8(\tau)}{3}\cos \hat{t} - \frac{S_9(\tau)\sin 2\hat{t}}{3} - \frac{S_{10}(\tau)}{8}\cos 3\hat{t} - \frac{S_{11}(\tau)\sin 3\hat{t}}{8} \quad (3.24)$$

Using the initial conditions, (3.31a) and (3.31g) in (4.24), gives

$$\eta^{32}(0,0) = a_{32}(0) + S_7(0) - \frac{S_8(0)}{3} - \frac{S_{10}(0)}{8} = 0; \therefore a_{32}(0) = 3bB(0)S_{15}$$

where,

$$S_{15} = \left[\frac{-24B(0)S_{12} + 8S_{13} + B(0)S_{14}}{24} \right]$$

4.3 The Maximum Displacement of the Model Problem

The displacement of $\eta(\hat{t}, \tau)$ can be written as

$$\eta(\hat{t}, \tau) = \epsilon(\eta^{10} + \delta\eta^{11} + \delta^2\eta^{12} + \dots) + \epsilon^2(\eta^{20} + \delta\eta^{21} + \delta^2\eta^{22} + \dots) + \epsilon^3(\eta^{30} + \delta\eta^{31} + \delta^2\eta^{32} + \dots) + \dots \quad (3.25a)$$

$$\text{But } \eta^{2j} = 0, \quad j = 0, 1, 2,$$

Therefore (3.25a) yields,

$$\eta(\hat{t}, \tau) = \epsilon(\eta^{10} + \delta\eta^{11} + \delta^2\eta^{12} + \dots) + \epsilon^3(\eta^{30} + \delta\eta^{31} + \delta^2\eta^{32} + \dots) + \dots \quad (3.25b)$$

The formula for determining the dynamic buckling load is given as

$$\frac{d\lambda}{d\eta_c} = 0 \quad (3.26)$$

where η_c is the maximum of $\eta(\hat{t}, \tau)$ and η_c is defined as $\eta(\hat{t}_c, \tau_c)$, where \hat{t}_c and τ_c are the critical values of \hat{t} and τ respectively at maximum displacement. We however

need to determine η_c first before invoking(3.26). It is to be recalled that, in terms of the original t – variable, the condition for maximum is

$$\frac{d\eta}{dt} = 0$$

However, the condition for maximum displacement interms of \hat{t} and τ is given as

$$\eta_{,\hat{t}} + \left(\frac{\mu'_2 \epsilon^2 + \mu'_3 \epsilon^3 + \dots}{(1 - \lambda \cos(\omega))^{1/2}} \right) \eta_{,\hat{t}} + \frac{\delta \eta_{,\tau}}{(1 - \lambda \cos(\omega))^{1/2}} = 0 \quad (3.27)$$

It is pertinent to assume the following asymptotic series

$$\hat{t}_c = (\hat{t}_0 + \delta \hat{t}_{01} + \delta^2 \hat{t}_{02} + \dots) + \epsilon(\hat{t}_{10} + \delta \hat{t}_{11} + \dots) + \epsilon^2(\hat{t}_{20} + \delta \hat{t}_{21} + \dots) + \dots \quad (3.28)$$

From (2.19b), we get,

$$\tau_c = \delta t_c \quad (3.29a)$$

where t_c is the critical value of t at maximum displacement. Expansion of t_c asymptotically, gives

$$t_c = (T_0 + \delta T_{01} + \delta^2 T_{02} + \dots) + \epsilon(T_{10} + \delta T_{11} + \dots) + \epsilon^2(T_{20} + \delta T_{21} + \dots) + \dots \quad (3.29b)$$

$$\therefore \tau_c = \delta t_c = \delta[(T_0 + \delta T_{01} + \dots) + \epsilon(T_{10} + \delta T_{11} + \dots) + \epsilon^2(T_{20} + \delta T_{21} + \dots)] \quad (3.29c)$$

At critical points, equation (3.27) gives

$$\eta_{,\hat{t}}(\hat{t}_c, \tau_c) + \left[\frac{\mu'_2(\tau_c)\epsilon^2 + \mu'_3(\tau_c)\epsilon^3 + \dots}{(1 - \lambda \cos \omega(\tau_c))^{1/2}} \right] \eta_{,\hat{t}}(\hat{t}_c, \tau_c) + \frac{\delta}{(1 - \lambda \cos \omega(\tau_c))^{1/2}} \eta_{,\tau}(\hat{t}_c, \tau_c) = 0 \quad (3.30)$$

The next thing is to expand (3.30) asymptotically using using (3.28), (3.29b, c) and obtain

$$\begin{aligned} & \epsilon[\eta_{,\hat{t}}^{10} + \{(\delta \hat{t}_{01} + \delta^2 \hat{t}_{02} + \dots) + \epsilon(\hat{t}_{10} + \delta \hat{t}_{11} + \delta^2 \hat{t}_{12} + \dots) + \epsilon^2(\hat{t}_{20} + \delta \hat{t}_{21} + \dots)\} \eta_{,\hat{t}}^{10} \\ & + \frac{1}{2}\{(\delta \hat{t}_{01} + \delta^2 \hat{t}_{02} + \dots) + \epsilon(\hat{t}_{10} + \delta \hat{t}_{11} + \delta^2 \hat{t}_{12} + \dots) + \epsilon^2(\hat{t}_{20} + \delta \hat{t}_{21} + \delta^2 \hat{t}_{22} + \dots)\}^2 \eta_{,\hat{t}\hat{t}}^{10} \\ & + \delta\{(T_0 + \delta T_{01} + \dots) + \epsilon(T_{10} + \delta T_{11} + \dots) + \epsilon^2(T_{20} + \delta T_{21} + \dots)\} \eta_{,\hat{t}\tau}^{10} \\ & + 2\delta\{(T_0 + \delta T_{01} + \dots) + \epsilon(T_{10} + \delta T_{11} + \dots) + \epsilon^2(T_{20} + \delta T_{21} + \dots)\} \{\delta \hat{t}_{01} + \dots \\ & + \epsilon(\hat{t}_{10} + \delta \hat{t}_{11} + \dots) + \epsilon^2(\hat{t}_{20} + \delta \hat{t}_{21} + \dots)\} \eta_{,\hat{t}\tau}^{10} + \delta^2\{T_0 + \dots + \epsilon(T_{10} + \dots) \\ & + \epsilon^2(T_{20} + \dots)\}^2 \eta_{,\hat{t}\tau}^{10}] + \epsilon \delta [\eta_{,\hat{t}}^{11} \{(\delta \hat{t}_{01} + \dots + \epsilon(\hat{t}_{10} + \delta \hat{t}_{11} + \dots)) + \epsilon^2(\hat{t}_{20} + \delta \hat{t}_{21} + \dots)\} \eta_{,\hat{t}\hat{t}}^{11} \\ & + \delta\{T_0 + \dots + \epsilon(T_{10} + \dots) + \epsilon^2(T_{20} + \dots)\} \eta_{,\hat{t}\tau}^{10} + \frac{1}{2}\{(\delta \hat{t}_{01} + \dots) + \epsilon(\hat{t}_{10} + \delta \hat{t}_{11} + \dots) \\ & + \epsilon^2(\hat{t}_{20} + \delta \hat{t}_{21} + \dots)\}^2 \eta_{,\hat{t}}^{11} + 2\delta\{(T_0 + \dots) + \epsilon(T_{10} + \dots) + \epsilon^2(T_{20} + \dots)\} \{\delta \hat{t}_{01} + \dots \\ & + \epsilon(\hat{t}_{10} + \delta \hat{t}_{11}) + \epsilon^2(\hat{t}_{20} + \delta \hat{t}_{21} + \dots)\} \eta_{,\hat{t}\tau}^{11}] + \epsilon \delta^2 [\eta_{,\hat{t}}^{12} + \{(\delta \hat{t}_{01} + \delta^2 \hat{t}_{02} + \dots) \\ & + \epsilon(\hat{t}_{10} + \dots) + \epsilon^2(\hat{t}_{20} + \dots)\} \eta_{,\hat{t}\hat{t}}^{12} + \dots] + \epsilon^3 [\eta_{,\hat{t}}^{30} + \{(\delta \hat{t}_{01} + \delta^2 \hat{t}_{02} + \dots)\} \eta_{,\hat{t}\hat{t}}^{30} + \delta\{T_0 + \delta T_{01} \\ & + \dots\} \eta_{,\hat{t}\tau}^{30} + \{\delta \hat{t}_{01} + \dots\}^2 \eta_{,\hat{t}\hat{t}\tau}^{30} + \dots] + \epsilon^3 \delta^2 [\eta_{,\hat{t}}^{30} + \dots] + \epsilon^3 \left[\frac{\mu'_2(0)\eta_{,\hat{t}}^{10}}{(1 - \lambda)^{1/2}} + \frac{\mu'_2(0)}{(1 - \lambda)^{1/2}} \{\delta \hat{t}_{01} \right. \\ & + \delta^2 \hat{t}_{02} + \dots\} \eta_{,\hat{t}\hat{t}}^{10} + \delta \left(\frac{\mu'_2(0)\eta_{,\hat{t}}^{10}}{1 - \lambda \cos(\omega)^{1/2}} \right)_{,\tau} \{T_0 + \delta T_{01} + \dots\} + \delta \left(\frac{\mu'_2(0)}{1 - \lambda \cos(\omega)^{1/2}} \right) \{T_0 + \delta T_{01} + \dots\} \\ & + \frac{1}{2} \left(\frac{\mu'_2(0)}{1 - \lambda \cos(\omega)^{1/2}} \right) \{\delta \hat{t}_{01} + \delta^2 \hat{t}_{02} + \dots\} \eta_{,\hat{t}\hat{t}}^{10} + 2\delta \left(\frac{\mu'_2(\tau)\eta_{,\hat{t}}^{10}}{1 - \lambda \cos(\omega)^{1/2}} \right)_{,\tau} \{T_0 + \dots\} \{\delta \hat{t}_{01} + \dots\} \left. \right] \\ & + \delta^2 \left\{ \left(\frac{\mu'_2(\tau)\eta_{,\hat{t}}^{10}}{1 - \lambda \cos(\omega)^{1/2}} \right)_{,\tau} (T_0 + \dots)^2 \right\} + \dots + \epsilon^2 \delta \left[\frac{\mu'_2(0)\eta_{,\hat{t}}^{11}}{(1 - \lambda)^{1/2}} + \frac{\mu'_2(0)}{(1 - \lambda)^{1/2}} \{\delta \hat{t}_{01} + \dots\} \eta_{,\hat{t}\hat{t}}^{11} \right. \\ & \left. + \delta \left(\frac{\mu'_2(\tau)\eta_{,\hat{t}}^{11}}{1 - \lambda \cos(\omega)^{1/2}} \right)_{,\tau} \{T_0 + \dots\} + \frac{1}{2} \left(\frac{\mu'_2(\tau)}{1 - \lambda \cos(\omega)^{1/2}} \right) \{\delta \hat{t}_{01} + \dots\} \eta_{,\hat{t}\hat{t}}^{11} \right] \end{aligned}$$

$$+2\delta \left(\frac{\mu'_2(\tau)\eta_{\hat{t}\hat{t}}^{11}}{1 - \lambda \cos(\omega)^{1/2}} \right)_{,\tau} (T_0 + \dots) \Bigg] + \epsilon^3 \delta^2 \left[\frac{\mu'_2(0)\eta_{\hat{t}}^{12}}{(1 - \lambda)^{1/2}} \right] = 0 \quad (3.31)$$

The next step is to proceed by equating (3.31) to zero in orders of $(\epsilon^i \delta^j)$ and obtain the following equations.

$$O(\epsilon): \eta_{\hat{t}}^{10} = 0; O(\epsilon\delta): \hat{t}_{01}\eta_{\hat{t}\hat{t}}^{10} + T_0\eta_{\hat{t}\tau}^{10} + \eta_{\hat{t}}^{11} + \frac{\eta_{,\tau}}{(1 - \lambda)^{1/2}} = 0 \quad (3.32a, b)$$

$$O(\epsilon\delta^2): \hat{t}_{02}\eta_{\hat{t}\hat{t}}^{10} + T_0\eta_{\hat{t}\tau}^{11} + \frac{\hat{t}_{02}}{2}\eta_{\hat{t}\hat{t}}^{10} + \hat{t}_{01}\eta_{\hat{t}\hat{t}}^{11} + \eta_{\hat{t}}^{12} + \frac{\hat{t}_{01}\eta_{\hat{t}\tau}^{10}}{(1 - \lambda)^{1/2}} + \frac{\eta_{,\tau}^{11}}{(1 - \lambda)^{1/2}} + T_0\eta_{\hat{t}\tau}^{10} + 2T_0\hat{t}_{01}\eta_{\hat{t}\tau}^{10} = 0 \quad (3.32c)$$

$$O(\epsilon^2): \hat{t}_{01}\eta_{\hat{t}\hat{t}}^{10} = 0; O(\epsilon^3): \hat{t}_{20}\eta_{\hat{t}\hat{t}}^{10} + \eta_{\hat{t}}^{30} + \frac{\mu'_2(0)\eta_{\hat{t}}^{10}}{(1 - \lambda)^{1/2}} = 0 \quad (3.32d, e)$$

$$O(\epsilon^3\delta): \hat{t}_{21}\eta_{\hat{t}\hat{t}}^{10} + T_{20}\eta_{\hat{t}\tau}^{10} + 2(T_0\hat{t}_{20} + T_{10}\hat{t}_{10})\eta_{\hat{t}\hat{t}\tau}^{10} + \hat{t}_{20}\eta_{\hat{t}}^{11} + \hat{t}_{01}\eta_{\hat{t}\hat{t}}^{30} + T_0\eta_{\hat{t}\tau}^{30} + \eta_{\hat{t}}^{31} + \frac{\hat{t}_{01}\mu'_2(0)\eta_{\hat{t}\hat{t}}^{10}}{(1 - \lambda)^{1/2}} + T_0 \left(\frac{\mu'_2(\tau)\eta_{\hat{t}}^{10}}{(1 - \lambda \cos(\omega))^{1/2}} \right)_{,\tau} + 2T_0\hat{t}_{01} \left(\frac{\mu'_2(\tau)\eta_{\hat{t}\hat{t}}^{10}}{(1 - \lambda \cos(\omega))^{1/2}} \right)_{,\tau} + \frac{\mu'_2(0)\eta_{\hat{t}}^{10}}{(1 - \lambda)^{1/2}} + \frac{\hat{t}_{20}\eta_{\hat{t}\tau}^{10}}{(1 - \lambda)^{1/2}} + \frac{\eta_{,\tau}^{30}}{(1 - \lambda)^{1/2}} = 0 \quad (3.32f)$$

$$O(\epsilon^3\delta^2): \hat{t}_{22}\eta_{\hat{t}\hat{t}}^{10} + T_{21}\eta_{\hat{t}\tau}^{10} + 2\hat{t}_{21}T_0\eta_{\hat{t}\hat{t}\tau}^{10} + T_{10}^2\eta_{\hat{t}\hat{t}\tau}^{10} + \hat{t}_{21}\eta_{\hat{t}\hat{t}}^{11} + T_{20}\eta_{\hat{t}\tau}^{11} + \hat{t}_{20}\eta_{\hat{t}}^{12} + \hat{t}_{02}\eta_{\hat{t}\hat{t}}^{30} + \hat{t}_{01}\eta_{\hat{t}\hat{t}}^{31} + T_0\eta_{\hat{t}\tau}^{31} + \eta_{\hat{t}}^{32} + \frac{\mu'_2(0)\hat{t}_{02}\eta_{\hat{t}\hat{t}}^{10}}{(1 - \lambda)^{1/2}} + T_{01} \left(\frac{\mu'_2(\tau)\eta_{\hat{t}}^{10}}{(1 - \lambda \cos(\omega))^{1/2}} \right)_{,\tau} + \left(\frac{\mu'_2(\tau)}{(1 - \lambda \cos(\omega))^{1/2}} \right) \frac{\hat{t}_{01}}{2} \eta_{\hat{t}\hat{t}\hat{t}}^{10} + 2T_0\hat{t}_{01} \left(\frac{\mu'_2(\tau)\eta_{\hat{t}\hat{t}}^{10}}{(1 - \lambda \cos(\omega))^{1/2}} \right)_{,\tau} + T_0^2 \left(\frac{\mu'_2(\tau)\eta_{\hat{t}}^{10}}{(1 - \lambda \cos(\omega))^{1/2}} \right)_{,\tau} + \hat{t}_{01} \left(\frac{\mu'_2(0)}{(1 - \lambda)^{1/2}} \right) \eta_{\hat{t}\hat{t}}^{11} + T_0 \left(\frac{\mu'_2(\tau)\eta_{\hat{t}}^{11}}{(1 - \lambda \cos(\omega))^{1/2}} \right)_{,\tau} + \frac{\mu'_2(0)\eta_{\hat{t}}^{11}}{(1 - \lambda)^{1/2}} + \frac{\hat{t}_{21}\eta_{\hat{t}\tau}^{10}}{(1 - \lambda)^{1/2}} + \frac{\hat{t}_{20}\eta_{\hat{t}\tau}^{11}}{1 - \lambda} + \frac{\eta_{,\tau}^{31}}{(1 - \lambda)^{1/2}} = 0 \quad (3.32g)$$

On solving (3.32a). that is,

$$\eta_{\hat{t}}^{10} = 0 \text{ and noting } \eta^{10}(\hat{t}, \tau) = a_{10}(\tau)\cos\hat{t} + B(\tau)$$

Hence,

$$\eta_{\hat{t}}^{10}(\hat{t}_0, 0) = -a_{10}(0)\sin\hat{t}_0 = 0; \sin\hat{t}_0 = 0 \text{ but } a_{10}(0) \neq 0; \therefore \hat{t}_0 = n\pi; n = 0, 1, 2, \dots$$

Since the aim is to look for a nontrivial solution, it is here necessary to take the *smallest non-trivial value of n*; which is $n = 1$, and obtain

$$\hat{t}_0 = \pi(3.32h)$$

The Solution of (3.32b) is

$$\hat{t}_{01} = \frac{1}{\eta_{\hat{t}\hat{t}}^{10}} \left[T_0\eta_{\hat{t}\tau}^{10} + \eta_{\hat{t}}^{11} + \frac{\eta_{,\tau}}{(1 - \lambda)^{1/2}} \right] (\hat{t}_0, 0)$$

$$\text{Since } \eta_{\hat{t}\tau}^{10}(\hat{t}_0, 0) = b_{11}(0) = \eta_{\tau}^{10} = 0$$

$$\therefore \hat{t}_{01} = 0 \quad (3.32i)$$

It is noted that,

$$\eta^{11}(\hat{t}_0, 0) = b_{11}(0)\cos\hat{t}_0 = 0; b_{11}(0)\cos\hat{t} = 0; b_{11}(0) = 0$$

Solving (3.32d), gives

$$\hat{t}_{10}\eta_{\hat{t}\hat{t}}^{10}(t_0, 0) = 0; \therefore \hat{t}_{10} = 0 \text{ but } \eta_{\hat{t}\hat{t}}^{10} \neq 0, \text{ also } \hat{t}_{02} = \hat{t}_{10} = \hat{t}_{11} = \hat{t}_{12} = \hat{t}_{20} = \hat{t}_{21} = \hat{t}_{22} = 0$$

The summary of the displacement so far is as follows;

$$\eta(\hat{t}, \tau) = \epsilon(\eta^{10} + \delta\eta^{11} + \delta^2\eta^{12} + \dots) + \epsilon^3(\eta^{30} + \delta\eta^{31} + \delta^2\eta^{32} + \dots) + \dots \quad (3.33)$$

Let $\eta_c = \eta(\hat{t}_c, \tau_c)$ be the maximum of $\eta(\hat{t}, \tau)$ and from (3.33), it is evident that,
 $\eta_c = \eta(\hat{t}_c, \tau_c) = \epsilon(\eta_c^{10} + \delta\eta_c^{11} + \delta^2\eta_c^{12} + \dots) + \epsilon^3(\eta_c^{30} + \delta\eta_c^{31} + \delta\eta_c^{32} + \dots) + \dots$ (3.34)

where;

$$\eta_c^{ij} = \eta^{ij}(\hat{t}_c, \tau_c) \quad (3.35)$$

Expanding each term of (3.35) asymptotically, gives the following

$$\begin{aligned} \epsilon\eta_c^{10} &= \epsilon[\eta^{10}(\hat{t}_0, 0) + \eta_{,\hat{t}}^{10}\{(\delta\hat{t}_{01} + \delta^2\hat{t}_{02} + \dots)\} + \epsilon(\hat{t}_{10} + \delta\hat{t}_{11} + \delta^2\hat{t}_{12} + \dots) \\ &+ \epsilon^2(\hat{t}_{20} + \delta\hat{t}_{21} + \delta^2\hat{t}_{22} + \dots)] + \eta_{,\tau}^{10} \delta\{(T_0 + \delta T_{01} + \dots) + \epsilon(T_{10} + \delta T_{11} + \dots) \\ &+ \epsilon^2(T_{20} + \delta T_{21} + \dots)\} + \frac{1}{2} \{ \eta_{,\hat{t}\hat{t}}^{10} \{ \delta\hat{t}_{01} + \delta^2\hat{t}_{02} + \dots \} + \epsilon(\hat{t}_{01} + \delta\hat{t}_{11} + \delta^2\hat{t}_{12} + \dots) \\ &+ \epsilon^2(\hat{t}_{20} + \delta\hat{t}_{21} + \delta^2\hat{t}_{22} + \dots) \}^2 + \delta\eta_{,\hat{t}\tau}^{10} \{ (T_0 + \delta T_{11} + \dots) + \epsilon(T_{10} + \delta T_{11} + \dots) \\ &+ \epsilon^2(T_{20} + \delta T_{21} + \dots) \} \{ \delta\hat{t}_{01} + \dots + \epsilon(\hat{t}_{01} + \delta\hat{t}_{01} + \dots) + \epsilon^2(\hat{t}_{20} + \delta\hat{t}_{21} + \dots) \} \\ &+ \delta^2\eta_{,\tau\tau}^{10} \{ (T_0 + \dots) + \epsilon(T_{10} + \dots) + \epsilon^2(T_{20} + \dots) \} \} \quad (3.36) \\ \epsilon\delta\eta_c^{11} &= \epsilon\delta[\eta^{11}(\hat{t}_0, 0) + \eta_{,\hat{t}}^{11}\{(\delta\hat{t}_{01} + \dots)\} + \epsilon(\hat{t}_{10} + \delta\hat{t}_{11} + \dots) + \epsilon^2(\hat{t}_{20} + \delta\hat{t}_{21} + \dots)] \\ &+ \eta_{,\tau}^{11} \delta\{(T_0 + \dots) + \epsilon(T_{10} + \dots) + \epsilon^2(T_{20} + \dots)\} + \frac{1}{2} \{ \eta_{,\hat{t}\hat{t}}^{11} \{ (\delta\hat{t}_{01} + \dots) \} + \epsilon(\hat{t}_{10} + \delta\hat{t}_{11} + \dots) \\ &+ \epsilon^2(\hat{t}_{20} + \delta\hat{t}_{21} + \dots) \}^2 + 2\delta\eta_{,\hat{t}\tau}^{10} \{ (\hat{t}_0 + \dots) + \epsilon(\hat{t}_{10} + \dots) + \epsilon^2(\hat{t}_{20} + \dots) \} \\ &+ \delta^2\eta_{,\tau\tau}^{12} \{ (T_0 + \dots) + \epsilon(T_{10} + \dots) + \epsilon(T_{20} + \dots) \} \} \quad (3.37) \end{aligned}$$

$$\epsilon\delta^2\eta_c^{12} = \epsilon\delta^2[\eta^{12}(\hat{t}_0, 0) + \eta_{,\hat{t}}^{12}\{\dots + \epsilon(\hat{t}_{10} + \dots) + \epsilon^2(\hat{t}_{20} + \dots)\}] \quad (3.38)$$

$$\epsilon^3\eta_c^{30} = \epsilon^3[\eta^{30}(\hat{t}_0, 0) + \eta_{,\hat{t}}^{30}\{(\delta\hat{t}_{01} + \delta^2\hat{t}_{02} + \dots)\} + \delta\eta_{,\tau}^{30}\{(T_0 + \delta T_{01} + \dots) + \dots\}] \quad (3.39)$$

$$\epsilon^3\delta\eta_c^{31} = \epsilon^3\delta[\eta^{31}(\hat{t}_0, 0) + \eta_{,\hat{t}}^{31}(\delta\hat{t}_{01} + \dots) + \delta\eta_{,\tau}^{31}\{(T_0 + \dots) + \dots\}] \quad (3.40)$$

$$\epsilon^3\delta^2\eta_c^{32} = \epsilon^3\delta^2[\eta^{32}(\hat{t}_0, 0) + \dots] \quad (3.41)$$

Grouping (3.36) to (3.41) in orders ($\epsilon^i \delta^j$), results to

$$\begin{aligned} \eta_c &= \epsilon \left[\eta^{10}(\hat{t}_0, 0) + \delta\{\hat{t}_0, \eta_{,\hat{t}}^{10} + \eta^{11}(\hat{t}_0, 0) + T_0\eta_{,\tau}^{10}\} + \delta^2 \left\{ \hat{t}_{02}\eta_{,\hat{t}}^{10} + T_{01}\eta_{,\tau}^{10} + \frac{\hat{t}_{01}}{2}\eta_{,\hat{t}\hat{t}}^{10} \right. \right. \\ &+ T_0\hat{t}_{01}\eta_{,\hat{t}\tau}^{10} + \frac{T_0^2}{2}\eta_{,\tau\tau}^{10} + \hat{t}_{01}\eta_{,\hat{t}}^{11} + T_0\eta_{,\tau}^{11} + \eta^{12}(\hat{t}_0, 0) \left. \left. \right\} + \dots + \epsilon^3 [\hat{t}_{20}\eta_{,\hat{t}}^{10} \right. \\ &+ \frac{\hat{t}_{01}}{2}\eta_{,\hat{t}\hat{t}}^{10} + \eta^{32}(\hat{t}_0, 0) + \delta\{\hat{t}_{21}\eta_{,\hat{t}}^{10} + T_{20}\eta_{,\tau}^{10} + \hat{t}_{11}\eta_{,\hat{t}}^{10} + T_0\hat{t}_{20}\eta_{,\hat{t}\tau}^{10} + \hat{t}_{20}\eta_{,\hat{t}}^{11} \\ &+ \frac{\hat{t}_{10}}{2}\eta_{,\hat{t}\hat{t}}^{11} + \hat{t}_{01}\eta_{,\hat{t}}^{30} + T_0\eta_{,\tau}^{30} + \eta^{31}(\hat{t}_0, 0) + \delta^2\{\hat{t}_{22}\eta_{,\hat{t}}^{10} + T_{21}\eta_{,\tau}^{10} + \frac{1}{2}\{2\hat{t}_{01}\hat{t}_{21} \\ &+ 2\hat{t}_{02}\hat{t}_{20} + \eta^{31}(\hat{t}_0, 0) + \hat{t}_{11}\}\}\eta_{,\hat{t}\hat{t}}^{10} + \{2(\hat{t}_{01}T_{20} + T_0\hat{t}_{21} + \hat{t}_{10}T_{11} + T_0\hat{t}_{11})\}\eta_{,\hat{t}\tau}^{30} \\ &+ T_{10}^2\eta_{,\tau\tau}^{11} + \hat{t}_{21}\eta_{,\hat{t}}^{11} + T_{20}\eta_{,\tau}^{11} + (\hat{t}_{01}\hat{t}_{20} + \hat{t}_{10}\hat{t}_{11})\eta_{,\hat{t}\hat{t}}^{11} + (\hat{t}_0\hat{t}_{20} + \hat{t}_{10}^2)\eta_{,\hat{t}\tau}^{11} + \hat{t}_{20}\eta_{,\hat{t}}^{12} \\ &+ \hat{t}_{02}\eta_{,\hat{t}}^{30} + T_{01}\eta_{,\tau}^{30} + \hat{t}_{01}\eta_{,\hat{t}}^{31} + T_0\eta_{,\tau}^{30} + \eta^{32}(\hat{t}_0, 0) \left. \right] \quad (3.42) \end{aligned}$$

Further simplification of (3.42) gives

$$\begin{aligned} \eta_c &= \epsilon \left[\eta^{10} + \delta^2 \left(\frac{T_0^2}{2}\eta_{,\tau\tau}^{10} + T_0\eta_{,\tau}^{11} + \eta^{12} \right) \right] (\hat{t}_0, 0) \\ &+ \epsilon^3 [\eta^{30} + \delta(T_0\eta_{,\tau}^{30} + \eta^{31}) + \delta^2(T_{20}\eta_{,\tau}^{11} + T_{01}\eta_{,\tau}^{30} + T_0\eta_{,\tau}^{31} + \eta^{32})] (\hat{t}_0, 0) + \dots \quad (3.43a) \end{aligned}$$

Substituting the values of $\eta^{ij}(\hat{t}_0, 0)$ in (3.43a), gives

$$\begin{aligned} \eta_c &= \epsilon \left[2B(0) + \delta^2 \left\{ \frac{T_0^2}{2} (\omega'^2(0)B(0) - \omega'^2(0)) + \frac{2\omega'^2(0)}{(1-\lambda)} \right\} \right] \\ &+ \epsilon^3 \left[\frac{67B^3(0)b}{32(1-\lambda)} - \frac{6\delta^2 b}{(1-\lambda)^3} (\omega'^2(0)B(0) - 2\omega'^2(0)B(0)) \right] + \dots \quad (3.43b) \end{aligned}$$

Equation(3.43b) contains the term T_0^2 which is yet to be determined. This term is now determined with recourse to (2.20c)

Thus at maximum displacement, the expansion of (2.20c) gives

$$\hat{t}_c = \tilde{t}_c + \frac{1}{\delta} \{ \mu_2(\tau)\epsilon^2 + \mu_3(\tau)\epsilon^3 + \dots \} \quad (3.44a)$$

Let,

$$\tilde{t}_c = \tilde{t}_0 + \delta \tilde{t}_{01} + \delta^2 \tilde{t}_{02} + \dots + \epsilon(\tilde{t}_{10} + \delta \tilde{t}_{11} + \delta^2 \tilde{t}_{12} + \dots) + \epsilon^2(\tilde{t}_{20} + \delta \tilde{t}_{21} + \dots) + \dots \quad (3.44b)$$

Expansion (4.44a), gives

$$\hat{t}_c = \tilde{t}_c + \frac{\epsilon^2}{\delta} \left[\mu_2(0) + \mu_2'(0)(\delta t_c) + \frac{1}{2} \mu_2''(0)(\delta t_c)^2 + \dots \right]; \quad \mu_2(0) = 0 \quad (3.44c)$$

$$\therefore \hat{t}_c = \tilde{t}_c + \epsilon^2 \left(\mu_2'(0)t_c + \frac{1}{2} \mu_2''(0)\delta t_c^2 + \dots \right) \quad (3.44d)$$

Expansion of both sides of (3.44d), gives

$$\begin{aligned} \hat{t}_0 + \delta \hat{t}_{01} + \delta^2 \hat{t}_{02} + \dots + \epsilon(\hat{t}_{10} + \delta \hat{t}_{11} + \delta^2 \hat{t}_{12} + \dots) + \epsilon^2(\hat{t}_{20} + \delta \hat{t}_{21} + \delta^2 \hat{t}_{22} + \dots) \\ = \tilde{t}_0 + \delta \tilde{t}_{01} + \delta^2 \tilde{t}_{02} + \dots + \epsilon(\tilde{t}_{10} + \delta \tilde{t}_{11} + \delta^2 \tilde{t}_{12} + \dots) + \epsilon^2(\tilde{t}_{20} + \delta \tilde{t}_{21} + \delta^2 \tilde{t}_{22} + \dots) \\ + \epsilon^2 [(\mu_2'(0))\{\tilde{t}_0 + \delta \tilde{t}_{01} + \dots + \epsilon^2(\tilde{t}_{20} + \delta \tilde{t}_{21} + \delta \tilde{t}_{22} + \dots) + \dots\}] \\ + \frac{\mu_2''(0)\delta}{2} [\tilde{t}_0 + \delta \tilde{t}_{01} + \delta^2 \tilde{t}_{02} + \dots + \epsilon(\tilde{t}_{10} + \delta \tilde{t}_{11} + \dots) + \epsilon^2(\tilde{t}_{20} + \delta \tilde{t}_{21} + \dots)]^2 \end{aligned} \quad (3.45)$$

On equating the orders of both sides, the result gives

$$O(1): \hat{t}_0 = \tilde{t}_0; O(\delta): \hat{t}_{01} = \tilde{t}_{01}; O(\delta^2): \hat{t}_{02} = \tilde{t}_{02}; O(\epsilon): \hat{t}_{10} = \tilde{t}_{10} \quad (3.46a, b, c, d)$$

$$O(\epsilon^2): \hat{t}_{20} = \tilde{t}_{20} + \mu_2'(0)\tilde{t}_0 \quad (3.46e)$$

It is to be recalled from(2.20b) that,

$$\frac{d\tilde{t}}{dt} = [1 - \lambda \cos(\omega(\delta t))]^{1/2} \quad (3.47)$$

Expansion of the right hand side of (3.47), gives

$$\frac{d\tilde{t}}{dt} = \left[1 - \lambda \left\{ 1 - \frac{\omega^2(\tau)}{2!} + \frac{\omega^4(\tau)}{4!} + \dots \right\} \right]^{1/2} = \left[(1 - \lambda) + \lambda \left\{ \frac{\omega^2(\tau)}{2} - \frac{\omega^4(\tau)}{4!} + \dots \right\} \right]^{1/2} \quad (3.48a)$$

Further simplification of (4.48a) using binomial expansion gives

$$\frac{d\tilde{t}}{dt} = (1 - \lambda)^{1/2} \left[1 + \frac{1}{2} \left(\frac{\lambda}{1 - \lambda} \right) \left\{ \frac{\omega^2(\tau)}{2!} - \frac{\omega^4(\tau)}{4!} + \dots \right\} - \frac{1}{8} \left(\frac{\lambda}{1 - \lambda} \right)^2 \left\{ \frac{\omega^2(\tau)}{2!} - \frac{\omega^4(\tau)}{4!} + \dots \right\}^2 \right] \quad (3.48b)$$

More expansion of (4.48b), gives

$$\begin{aligned} \frac{d\tilde{t}}{dt} = (1 - \lambda)^{1/2} \left[1 + \frac{1}{2} \left(\frac{\lambda}{1 - \lambda} \right) \left\{ \frac{\omega^2(0)}{2} + \frac{(\omega^2)'(0)}{1!} \delta t + \frac{(\omega^2)''(0)}{2!} (\delta t)^2 + \dots \right\} \right. \\ \left. - \frac{1}{8} \left(\frac{\lambda}{1 - \lambda} \right)^2 \frac{1}{2} \left\{ \omega^2(0) + \frac{(\omega^2)'(0)}{1!} \delta t + \frac{(\omega^2)''(0)}{2!} (\delta t)^2 + \dots \right\}^2 \right. \\ \left. - \frac{1}{4!} \left[\omega^4(0) + \frac{(\omega^4)'(0)\delta t}{1!} + \frac{(\omega^4)''(0)(\delta t)^2}{2!} + \dots \right] - \frac{1}{4!} \left\{ \omega^4(0) + \frac{\omega'^4(0)\delta t}{1!} + \frac{\omega''^4(0)(\delta t)^2}{2!} + \dots \right\}^2 \right] \end{aligned} \quad (3.48c)$$

Further simplification (3.48c) gives

$$\begin{aligned} \frac{d\tilde{t}}{dt} = (1 - \lambda)^{1/2} \left[\left\{ 1 + \frac{\lambda}{2(1 - \lambda)} \left\{ \frac{1}{2} \omega^2(0) - \frac{1}{4!} \omega^4(0) \right\} \right\} - \frac{1}{8} \left(\frac{\lambda}{1 - \lambda} \right)^2 \left\{ \frac{1}{4} \omega^4(0) - \frac{\omega^8(0)}{(4!)^2} \right\} \right. \\ \left. + \left\{ \frac{-\lambda}{2(1 - \lambda)} \left(\frac{(\omega^2)'(0)}{2} - \frac{(\omega^4)'(0)}{4!} \right) - \frac{1}{8} \left(\frac{\lambda}{1 - \lambda} \right)^2 \right\} \right] + \left\{ \frac{\omega^2(0)\omega'^2(0)}{2} - \frac{\omega^4(0)\omega'^4(0)}{288} \right. \\ \left. - \frac{\omega^2(0)\omega'^4(0)}{1152} - \frac{\omega'^2(0)\omega^4(0)}{1152} \right\} \delta t + \left\{ \left\{ -\frac{1}{8} \left(\frac{\lambda}{1 - \lambda} \right)^2 \left\{ \frac{(\omega^2)'(0)}{3} + \frac{\omega^2(0)(\omega^2)''(0)}{2} \right\} - \left(\frac{(\omega^4)'(0)}{576} \right)^2 \right. \right. \end{aligned}$$

$$\left. -\frac{\omega^3(0)\omega''^4(0)}{576} - \frac{\omega^2(0)\omega''^4(0)}{24} - \frac{\omega'^2(0)\omega^2(0)}{24} - \frac{\omega''^2(0)\omega^3(0)}{48} \right\} (\delta t)^2 + \dots \quad (3.48d)$$

Now (3.48d) can be written simply as

$$\frac{d\tilde{t}}{dt} = (1 - \lambda)^{1/2} [\beta_1 + \beta_2 \delta t + \beta_3 (\delta t)^2 + \dots] \quad (3.49)$$

where,

$$\beta_1 = \left[1 + \frac{\lambda}{2(1-\lambda)} \left\{ \frac{\omega^2(0)}{2} - \frac{\omega^4(0)}{24} \right\} - \frac{1}{8} \left(\frac{\lambda}{1-\lambda} \right)^2 \left\{ \frac{\omega^4(0)}{4} - \frac{\omega^8(0)}{576} \right\} \right] \quad (3.50a)$$

$$\beta_2 = \left[\frac{-\lambda}{2(1-\lambda)} \left\{ \frac{(\omega^2)'(0)}{2} - \frac{(\omega^4)'(0)}{576} \right\} - \frac{1}{8} \left(\frac{\lambda}{1-\lambda} \right)^2 \left\{ \frac{\omega^2(0)(\omega^2)'(0)}{2} - \frac{\omega^4(0)(\omega^4)'(0)}{288} \right\} - \frac{\omega^2(0)\omega'(0)}{1152} \right] \quad (3.50b)$$

$$\beta_3 = -\frac{1}{8} \left(\frac{\lambda}{1-\lambda} \right)^2 \left[\frac{(\omega^2)'(0)}{3} + \frac{\omega^2(0)(\omega^2)''(0)}{2} - \frac{(\omega^4)'(0)}{576} - \frac{\omega^4(0)(\omega^4)''(0)}{576} - \frac{(\omega^2)'(0)(\omega^4)''(0)}{24} - \frac{(\omega^2)''(0)\omega^4(0)}{488} \right] \quad (3.50c)$$

From (3.49), it follows that,

$$d\tilde{t} = (1 - \lambda)^{1/2} [\beta_1 + \beta_2 \delta t + \beta_3 (\delta t)^2 + \dots] dt \quad (3.51a)$$

integrating both sides of (3.51a), gives

$$\tilde{t} = (1 - \lambda)^{1/2} \left[\beta_1 t + \frac{1}{2} \beta_2 \delta t^2 + \frac{\beta_3}{3} \delta^2 t^3 + \dots \right] \quad (3.51b)$$

Thus, using (3.51b), it follows that,

$$\tilde{t}_c = (1 - \lambda)^{1/2} \left[\beta_1 t_c + \frac{\beta_2 \delta t_c^2}{2} + \frac{\beta_3 \delta^2 t_c^3}{3} + \dots \right] \quad (3.51c)$$

The term \tilde{t}_c can be expanded as

$$\tilde{t}_c = (\tilde{t}_0 + \delta \tilde{t}_{01} + \delta^2 \tilde{t}_{02} + \dots + \epsilon (\tilde{t}_{10} + \delta \tilde{t}_{11} + \delta^2 \tilde{t}_{12} + \dots) + \epsilon^2 (\tilde{t}_{20} + \delta \tilde{t}_{21} + \dots) + \dots$$

While it is to be recalled from (3.29b) that

$$t_c = T_0 + \delta T_{01} + \delta^2 T_{02} + \dots + \epsilon (T_{10} + \delta T_{11} + \delta^2 T_{12} + \dots) + \epsilon^2 (T_{20} + \delta T_{21} + \delta^2 T_{22} + \dots) + \dots$$

By asymptotic expansion of both sides of (3.51c), the result gives

$$\begin{aligned} & \tilde{t}_0 + \delta \tilde{t}_{01} + \delta^2 \tilde{t}_{02} + \dots + \epsilon (\tilde{t}_{10} + \delta \tilde{t}_{11} + \delta^2 \tilde{t}_{12} + \dots) + \epsilon^2 (\tilde{t}_{20} + \delta \tilde{t}_{21} + \delta^2 \tilde{t}_{22} + \dots) + \\ & = (1 - \lambda)^{1/2} [\beta_1 \{T_0 + \delta T_{01} + \delta^2 T_{02} + \dots + \epsilon (T_{10} + \delta T_{11} + \delta^2 T_{12} + \dots) + \epsilon^2 (T_{20} + \delta T_{21} \\ & + \delta^2 T_{22} + \dots)\} + \frac{\beta_2 \delta}{2} [(T_0 + \delta T_{01} + \delta^2 T_{02} + \dots) + \dots + \epsilon (T_{10} + \delta T_{11} + \delta^2 T_{12} + \dots) \\ & + \epsilon^2 (T_{20} + \delta T_{21} + \delta^2 T_{22} + \dots)]^2 + \frac{\beta_3 \delta^2}{3} [(T_0 + \delta T_{01} + \dots) \\ & + \epsilon (T_{10} + \delta T_{11} + \dots) + \epsilon^2 (T_{20} + \delta T_{22} + \dots)]^3 \end{aligned} \quad (3.51d)$$

On equating the orders of both sides of (4.51d), the following are obtained

$$O(1): \tilde{t}_0 = (1 - \lambda)^{1/2} \beta_1 T_0; O(\delta): \tilde{t}_{01} = (1 - \lambda)^{1/2} \left[\beta_1 T_{01} + \frac{\beta_2 T_0}{2} \right] \quad (3.52a, b)$$

$$O(\delta^2): \tilde{t}_{02} = (1 - \lambda)^{1/2} [\beta_1 T_{02} + \beta_2 T_0 T_{01}]; O(\epsilon): \tilde{t}_{10} = (1 - \lambda)^{1/2} \beta_1 T_{10} \quad (3.52c, d)$$

$$O(\epsilon \delta): \tilde{t}_{11} = (1 - \lambda)^{1/2} [\beta_1 T_{11} + \beta_2 T_0 T_{01}] \quad (3.52e)$$

$$O(\epsilon \delta^2): \tilde{t}_{12} = (1 - \lambda)^{1/2} [\beta_1 T_{12} + \beta_2 (T_0 T_{11} + T_{01} T_{10})]; O(\epsilon^2): \tilde{t}_{20} = (1 - \lambda)^{1/2} \beta_1 T_{20} \quad (3.52f, g)$$

$$O(\epsilon^2 \delta): \tilde{t}_{21} = (1 - \lambda)^{1/2} \left[\beta_1 T_{21} + \frac{\beta_2}{2} (T_{10}^2 + 2T_{10} T_{20}) \right] \quad (3.52h)$$

$$O(\epsilon^2 \delta^2): \tilde{t}_{22} = (1 - \lambda)^{1/2} [\beta_1 T_{22} + \beta_2 (T_0 T_{21} + T_{10} + T_{11} + T_0 T_{21} + T_{01} T_{20})] \quad (3.52i)$$

Substituting from (3.46a), (3.32b), $\tilde{t}_0 = \pi$ in (3.52a), gives,

$$T_0 = \frac{\pi}{\beta_1(1-\lambda)^{1/2}}, \text{ also, } T_{01} = \frac{\beta_2\pi^2}{2\beta_1^3(1-\lambda)}; T_{02} = -\frac{\beta_2\pi^3}{2\beta_1^5(1-\lambda)^{5/2}} \quad (3.53a, b, c)$$

From (3.52d), it follows that,

$$T_{10} = 0; \text{ since } \tilde{t}_{10} = 0, \text{ also, } T_{11} = T_{12} = T_{20} = T_{21} = T_{22} = 0$$

Hence, we have determined T_0, T_{01} and T_{20} which are to be substituted in (3.43a)

On expansion of (3.43b), the results gives

$$\eta_c = \left[2B(0) + \delta^2 \left\{ \frac{T_0^2}{2} \left(\frac{\omega'^2(0)B(0) - \omega'^2(0)}{(1-\lambda)} \right) + \frac{2\omega'^2(0)}{(1-\lambda)} \right\} \right] + \epsilon^2 \left[\frac{67B^2(0)b}{32(1-\lambda)} - \frac{6\delta^2 b}{(1-\lambda)^3} \{ \omega'^2(0)B(0) - 2B^2(0)\omega'^2(0) \} \right]$$

This can be recasted as

$$\eta_c = \epsilon G_1 + \epsilon^2 G_2 + \dots \quad (3.54)$$

where,

$$G_1 = 2B(0) \left[1 + \frac{\delta^2 \omega'^2(0)}{4(1-\lambda)B(0)} \{ B(0) - 1 \} T_0^2 + 4 \right] \quad (3.55a)$$

$$G_2 = \frac{67B^3(0)b}{32(1-\lambda)} \left[1 + \frac{192\delta^2 \omega'^2(0)(2B(0) - 1)}{67B^2(0)(1-\lambda)^2} \right] \quad (3.55b)$$

Further simplification (3.55a, b) gives;

$$G_1 = 2B(0)(1 + d_1\delta^2); G_2 = \frac{67B^3(0)b}{32(1-\lambda)}(1 + d_2\delta^2) \quad (3.56a, b)$$

where,

$$d_1 = \frac{\omega'^2(0)}{4(1-\lambda)B(0)} \{ (B(0) - 1)T_0^2 + 4 \}; \quad d_2 = \frac{192\omega'^2(0)}{67B^2(0)(1-\lambda)^2} (2B(0) - 1) \quad (3.57a, b)$$

3.4 Dynamic buckling load of the model structure

According to Amazigo and Ette (1987), the procedure for finding the dynamic buckling load λ_D , involves first reversing the series in (3.54) as follows:

$$\epsilon = k_1\eta_c + k_3\eta_c^3 + \dots \quad (3.58)$$

Such a reversal of series is required in order to ensure the boundedness of solution after buckling

Substituting for η_c in (3.58) using (3.54) results to

$$\epsilon = k_1(\epsilon G_1 + \epsilon^3 G_3 + \dots) + k_3(\epsilon G_1 + \epsilon^3 G_3 + \dots)^3 + \dots \quad (3.59)$$

Equating the coefficients of ϵ in (3.59), leads to

$$k_1 G_1 = 1. \therefore k_1 = \frac{1}{G_1} \quad (3.60a)$$

Equating the coefficient of ϵ^3 in (3.59), results to

$$k_1 G_3 + k_3 G_1^3 = 0. \therefore k_3 = -\frac{k_1 G_3}{G_1^3} = -\frac{G_3}{G_1^4} \quad (3.60b)$$

To obtain the dynamic buckling load λ_D , it is necessary to invoke (3.26) and obtain

$$\frac{d\epsilon}{d\eta_c} = \frac{d}{d\eta_c} [k_1\eta_c + k_3\eta_c^3 + \dots]; \frac{d\epsilon}{d\eta_c} = 0; \epsilon \text{ (constant)} \quad (3.61a)$$

$$\therefore \frac{d(k_1)}{d\lambda} \frac{d\lambda}{d\eta_c} \eta_c + k_1 \frac{d\eta_c}{d\eta_c} + \frac{d(k_3)}{d\lambda} \frac{d\lambda}{d\eta_c} \eta_c^3 + \frac{k_3 d(\eta_c^3)}{d\eta_c} = 0 \quad (3.61b)$$

From (3.61b), it follows that

$$k_1 + 3k_3\eta_c^2 + \dots = 0; \left(\text{since } \frac{d\lambda}{d\eta_c} = 0 \right); \lambda = \lambda_D; \text{ and } k_1(\lambda_D) + 3k_3(\lambda_D)\eta_{cD}^2 = 0 \quad (3.61c, d)$$

where,

$$\eta_{cD} = \eta_c(\lambda_D). \therefore \eta_{cD} = \left(\frac{-k_1(\lambda_D)}{3k_3(\lambda_D)} \right)^{1/2} = \left(\frac{-k_1}{3k_3} \right)^{1/2} \quad (3.61e)$$

Substituting the values of k_1 and k_3 respectively in (3.61e), leads to

$$\eta_{CD} = \left(\frac{G_1^3}{3G_3} \right)^{1/2} \quad (3.61f)$$

where, η_{CD} is the displacement at buckling. To determine the dynamic buckling load λ_D , there is need to evaluate (3.58) at buckling and get,

$$\epsilon = k_1(\lambda_D)\eta_{CD} + k_3(\lambda_D)\eta_{CD}^3 + \dots \quad (3.62)$$

Substituting the values of k_1 and k_3 and η_{CD} in (3.62), results to

$$\epsilon = \frac{2}{3\sqrt{3}} \sqrt{\frac{G_1}{G_3}}; \epsilon = \frac{2}{3\sqrt{3}} \left[\frac{2B(0)}{\frac{67B^2(0)b}{32(1-\lambda)}} \left(\frac{1+d_1\delta^2}{1+d_2\delta^2} \right) \right]^{1/2} \quad (3.63a, b)$$

Further simplification of (3.63b) gives

$$(1 - \lambda_D)^{3/2} = \frac{3\sqrt{201}}{16} \lambda_D b^{1/2} \epsilon Z^{1/2}; \text{ and } Z = \left(\frac{1+d_2\delta^2}{1+d_1\delta^2} \right) \quad (4.64)$$

CONCLUSION

Hence, we see that the dynamic buckling load, λ_D depends on the first derivative of the circular frequency evaluated at the initial time. We found that the least order of dependence of λ_D on δ is of the form δ^2 (4.64). Hence, if δ is very small compared to unity i. e. $0 < \delta \ll 1$, then δ^2 is even smaller and generally tends to zero. Thus, periodic loading with slowly varying circular frequency tends to a step load. The equation (4.46) is the expected load equation and λ_D is dynamic buckling load.

REFERENCES

- [1] Budiansky, B. (1966), *dynamic buckling of elastic structures; criteria and estimates in dynamic stability of structures*, pergamon, new York
- [2] Hutchison, J. W. & Budiansky, B. (1966); *dynamic buckling estimates*, A.I.A.A.J, 4, 525-530.
- [3] Danielson, D. (1969); *dynamic buckling loads of imperfection – sensitive structures from procedures*, A.I.A.A.J, 7, 1506-1510.
- [4] Collinge, I. R. & Ockendon, J. R. (1974); *transition through resonance of a Duffing oscillator*, STAM Journal of Applied Mathematics 37(2), 350 – 357.
- [5] Mania, R.J. (2010), *dynamic buckling of thin – walled viscoplastic columns (in polish); scientific Bulletin of Lodz. Technical University, Lodz.*
- [6] Kowal – Michalska, K. & Mania, R. (2008), *some aspects of dynamic buckling of plates under in-plane compression*, mechanics and Mechanical Engineering, 12(8), 135-146.
- [7] Kowal – Michalska, K. (2010), *About some important parameters in dynamic buckling analysis of plated structure subjected to pulse loading*, Mechanics and Mechanical Engineering, 14(2), 269-279.
- [8] Ette, A.M. Chukwuchekwa, J.U., Osuji, W.I., Udo-Akpan, I.U., & Ozoigbo, G.E. (2018). Asymptotic investigation of the buckling of a cubic – Quintic nonlinear elastic model structure stressed by static load and A Dynamic Step Load. *IOSR Journal of Mathematics (IOSR-JM) e-ISSN: 2278-5728, pp-ISSN: 2319-765X.14(1), 16-30.*
- [9] Erneux, T. & Mandel, P. (1986), *imperfect bifurcation with slowly varying control*. SIAM parameter journal on applied Mathematics 46(1), 1-15.
- [10] Belyaev, A.K., Ilin, D.N. & Morozov N.F. (2013); *Stability of transverse vibration of rod under longitudinal step-wise loading*. journal of Physics: Conference series 451 (2013) 012023 (DOI: 10:1088/1742 – 6596/451/1/012023).
- [11] Thompson, J.M. (2014); *advances in shell buckling: theory and experiments, lecture on Gabor Stephan's 60th birthday held July 3-5, 2014, Budapest.*

- [12] Goncalves, P. B. & Santee D.M. (2008); *Influence of uncertainties on the dynamic buckling loads of structures liable to asymmetric post buckling behavior*. Hindawi publishing corporation *Mathematical problems in engineering* vol. 2008, article ID490137, 240 pages. (DOI:10, 115/2008/490137).
- [13] Bhoi,R.M.&Kalurkar,L. G.(2014), *Study of buckling behavior of beam and Column*. *IOSR journal of Mechanical and Civil engineering (IOSR - JMCE)* e-ISSN; 2278-1684, P-ISSN: 2320-334X, 4(1),36 -40.
- [14] Vaughn D. G. & Hutchison J. W. (2006); *Buckling – waves*. *European journal of mechanics/Solids*, 25(2006) 1-12.
- [15] Udo – Akpan, I.U. &Ette, A. M. (2016); *on the dynamic buckling of a model structure with quadratic non-linearity struck by a step load superposed on a Quasi – Static load*. *Journal of the Nigerian Association of Mathematical physics*, 35, 461-472.
- [16] Reda, A.M. & Forbes, G.L. (2012); *investigation into the dynamic effect of lateral buckling of high temperature/high pressure offshore pipe lines*, *proceedings of Acoustic*, paper 83, Australia.
- [17] Pi, Y-L & Bradford, M.A. (2008); *dynamic buckling of shallow pin ended arches under a sudden central concentrated load*, *journal of sound and vibration*, 317(3-5).
- [18] AvarMechmet (2004), *elastic bucking of steel columns Under axial Compression*. *American Journal of civil Engineering*, 2(3),102-108.
- [19] Adman, R. &Saidani, M. (2003); *Elastic Buckling of Columns with end restraint effect*, *journal of Constructural steel research*, 87, 1-5.
- [20] Huang,Y. &Li,X.F.(2012);*An analytic approach for exactly determining critical loads of buckling of non-uniform columns*. *Int. Journal of structural stability and dynamics*12(4), id1250027.
- [21] Darbandi, S. M, Frouz-Abadi, R. D &Haddapour. H, (2010) *Buckling of variable section columns under axial loading*. *Journal of engineering Mechanics – ASCE*,136(4), 472-476.
- [22] Osuji A.C, Ette, A.M. and Chukwuchekwa, J.U. (2016); *Perturbation technique in the buckling of a Cubic model struck by a periodic load with slowly varying frequency*. *J. of the Nigerian association of Mathematical physics*, 37,71-90.
- [23] Morozov, N.F. &Tovstik P.E (2009); *dynamic of rod under axial impact (in Russian)* *vestnik of St. Petersburg State University, series 1105-11*.
- [24] Lee, B.K. Lee, T.E &Jaung, Y.S. (2012), *Numerical methods for determining strongest cantilever beam with constant volume*, *KSCS journal of civil Engineering*, 16(1), 169-178.
- [25] Capiez Lernout, E., Soize, C. &Mignolef, M.P. (2013); *Non linear stochastic dynamical post buckling analysis of uncertain cylindrical shells*, *11th International conference on recent advanced instructural Dynamics, RASD, 2013, Pisa, Italy*.
- [26] Chitra, V. &Priyadarasini, R. S. (2013); *Dynamic buckling of composite cylindrical shells subjected to axial impulse*, *Int. Journal of Scientific & Engineering Research* 4(5), 162 – 165.
- [27] Priyadarasini, R. S., Kalyangraman, V. &Srinyasam, S.M. (2012); *Numerical and experimental stability of buckling of advanced fibre composite cylinders under axial compression*, *Int. J. of structural stability and dynamic* 12(4), 1-25.
- [28] Mcshane, G.J., Pingle, S.M, Deshpande & Fleck, N.A. (2012); *dynamic buckling of a structure*, *Int. journal of solids and structures*, 49, 2830-2838.
- [29] Batra,R.C.&Wei Z. G.(2015); *Dynamic buckling of a thin thermoliscophstric rectangular plate*.*J. of thin – walled struct.* 2005, 43, 273 – 290.
- [30] Ette, A. M,Chukwuchekwa,J. U. &Udo–Akpan,I.(2016);*The buckling of a damped viscously damped column trapped by a step load*, *International J. Applied Sciences and Mathematics*, 3(2) 117-123.
- [31] Coskun, S.B. (2010), *Analysis of tilt – buckling of Euler column with varying flexural stiffens using homotopy perturbation method*. *Mathematical modeling and analysis*, 15(3), 275 – 286.

- [32] Ibrahim, A.M, Ozturk, H., &Sabuncu, M. (2013) *vibration analysis of cracked frame structures. Structural Engineering and Machines* 45(1),33-52.
- [33] Tekeli, H., Kormaz, K.A., Demir, F. &carhoglu, A.I. (2014); *comparison of critical column buckling load in regression, Fuzzy logic and ANN based estimates, journal of intelligent and Fuzzy systems*, 26(3),1077-1087.
- [34] Kumar, M. &Yadar, N. (2013), *buckling analysis of a beam – column using multilayer perception neural network technique, journal of the Franklin Mathematics*, 350(10), 3188-3204.
- [35] Okay, F., Atay, M. T. &Cockun, S.B. (2010), *determination of buckling loads and mode shapes of a heavy vertical column underweight using the variational iteration method, international journal of non-linear sciences and numerical simulation*,11(10), 851-857.
- [36] Yuan, W. B., Kim, B. & Li, L – Y (2014); *buckling of axially loaded castellated steel columns. Journal of constructional steel research*, 92, 40-45.
- [37] Huang Y. &Luo Q. Z. (2011); *a simple method to determine the critical buckling loads for axially in homogenous beams with elastic restraint. Computers and mathematics with Applications*, 62(12), 2510-2517.
- [38] AytekinEryilmaz, M. Tarik Atey, Safa B. Coskun&Musa Basbiik (2013), *buckling of Euler columns with a continuous elastic restraint via homotopy analysis method, Hindawi Publishing corporation journal of applied Mathematics volume 2013 article ID341063, 8 pages [http://dx. doi.org/10.1155/2013/341063](http://dx.doi.org/10.1155/2013/341063)*
- [39] Esen, T. (2015),*Anew FEM procedure for transverse and longitudinal vibration analysis of thin rectangular moving load along an arbitrary trajectory. Latin American journal of solids and structures* 12,808-830.
- [40] Chukwuchekwa, J. U. &Ete, A. M. (2015); *Asymptotic analysis of an improved quadratic model structure subjected to static loading, journal of the Nigeria Association of Mathematical Physics*, 32,237-244.
- [41] Jatar, S.K. &Dalta, P.K. (2014), *shape optimization of damage columns subjected to conservation and non-conservative forces. Int. Journal of Aeronautical and space Sciences*, 15(1), 20-31.
- [42] Ohsaki M. (2014), *Maximum load factor corresponding to a slightly asymmetric bifurcation point, Int. J. of Mechanical Sciences* 46(11) 1621-1634.
- [43] Bisagni, C., &Vescovini, R. (2009), *analytical formulation for local buckling and post buckling analysis of stiffened laminated panels. Thin – walled structures*, 47, 318 – 334.
- [44] Atanacko-vic, T.M (2007); *Optimal shape of a Strongest invested Column. Journal of Computational and applied Mathematics*, 203(1),209-218.